

A Table of \$\surd \$(\$\frac{1}{2}\pi \$) e\$^{\frac{1}{2}i\pi \rho ^{2}}\int_{\rho}^{\infty}\$ e\$^{-\frac{1}{2}i\pi \lambda ^{2}}\$ d \$\lambda \$ for Complex Values of \$\rho \$

P. C. Clemmow and Cara M. Munford

Phil. Trans. R. Soc. Lond. A 1952 **245**, 189-211 doi: 10.1098/rsta.1952.0022

Email alerting service

Receive free email alerts when new articles cite this article - sign up in the box at the top right-hand corner of the article or click **here**

To subscribe to Phil. Trans. R. Soc. Lond. A go to: http://rsta.royalsocietypublishing.org/subscriptions

TRANSACTIONS CONTENT

SOCIFTV

[189]

A TABLE OF $\sqrt{(\frac{1}{2}\pi)} e^{\frac{1}{2}i\pi\rho^2} \int_{0}^{\infty} e^{-\frac{1}{2}i\pi\lambda^2} d\lambda$ FOR COMPLEX VALUES OF ρ

By P. C. CLEMMOW, Cavendish Laboratory, Cambridge AND CARA M. MUNFORD, Mathematical Laboratory, Cambridge

(Communicated by D. R. Hartree-Received 16 April 1951-Tables checked in proof 2 July 1952)

In the theory of wave propagation the above function has applications for which ρ may be complex within a certain range of argument. Tables of the real and imaginary parts of the function are given to four decimal places, for values of $|\rho|$ from 0 to 0.80 at intervals of 0.01, and for values of arg ρ from 0° to 45° at intervals of 1°.

1. INTRODUCTION

The tabulation of functions for complex values of their argument is very seldom undertaken. This fact is, perhaps, not surprising in view of the enormous increase of labour involved when the argument has two degrees of freedom. It is, however, unfortunate that the widespread use of the complex variable in mathematical physics cannot be more adequately supported by numerical tables. The deficiency is particularly noticeable in wave theory; here the complex variable is an essential tool, but both the relatively simple form and the physical content of a result may be destroyed by the necessity of separating it into real and imaginary parts for the purpose of computation.

In the course of recent work on wave propagation, one of the authors has become convinced of the desirability of tabulating a function allied to the complex Fresnel integral for complex values of the argument. The tables given here are a partial fulfilment of this requirement. There follows a brief description of the function, together with an indication of the type of problem in which it will be useful.

2. The function

Although the general nature of a function for which numerical values are required may be clear, there is often some arbitrariness in the choice of the exact form to be adopted for tabulation. This is the case here. We have said that the function with which we are concerned is related to the complex Fresnel integral, but to-day this term might imply any one of the four following integrals:

$$\int_0^\rho e^{-i\lambda^2} d\lambda, \tag{1}$$

$$\int_0^{\rho} \mathrm{e}^{-\frac{1}{2}i\pi\lambda^2} d\lambda,\tag{2}$$

$$\int_{\rho}^{\infty} \mathrm{e}^{-i\lambda^2} d\lambda, \tag{3}$$

$$\int_{\rho}^{\infty} e^{-\frac{1}{2}i\pi\lambda^2} d\lambda, \qquad (4)$$

[Published 16 September 1952

Vol. 245. A. 895. (Price 5s. 6d.)

23



190 P. C. CLEMMOW AND CARA M. MUNFORD

omitting minor variations such as changing the sign of i. The distinction between (1) and (2) is unimportant, as is likewise that between (3) and (4). On the other hand, (3) and (4) arise more directly in physical applications than (1) and (2) respectively.

When the Fresnel integrals were originally introduced, only real values of the argument were considered. The functions (1) to (4) may be conveniently tabulated for real values of ρ ; but when ρ is complex within a range of argument to be discussed in the next section, (1) to (4) are not suitable for tabulation. The inclusion of an appropriate exponential factor, however, yields functions which are free of this defect; and, indeed, it is these new functions, rather than (1) to (4) themselves, which appear in physical problems.

The above considerations led to the choice of

$$G(\rho) = e^{\frac{1}{2}i\pi\rho^2} \int_{\sqrt{(\frac{1}{2}\pi)\rho}}^{\infty} e^{-i\lambda^2} d\lambda = \sqrt{(\frac{1}{2}\pi)} e^{\frac{1}{2}i\pi\rho^2} \int_{\rho}^{\infty} e^{-\frac{1}{2}i\pi\lambda^2} d\lambda$$
(5)

as the function to be tabulated for complex values of ρ . The function of z obtained from (5) by writing $\rho = \sqrt{2/\pi} z$ has a slightly simpler mathematical form, but the adoption of ρ rather than z as the argument is in accord with most of the existing tables of Fresnel integrals.

3. The range of argument

In the physical applications which we have in mind it is found that $0 \leq \arg \rho \leq \frac{1}{4}\pi$, and the tabulation of (5) has therefore been confined to values of $\arg \rho$ within this range. The asymptotic expansion of (5) for large values of $|\rho|$ is then

$$G(\rho) \sim \frac{1}{i\sqrt{(2\pi)}\,\rho} \bigg[1 - \frac{1}{i\pi\rho^2} + \frac{1\cdot3}{(i\pi\rho^2)^2} - \frac{1\cdot3\cdot5}{(i\pi\rho^2)^3} + \dots \bigg],\tag{6}$$

which shows how the behaviour of (5) as $|\rho| \rightarrow \infty$ compares favourably with that of the same function without the factor exp $(\frac{1}{2}i\pi\rho^2)$.

The values of $|\rho|$ in the tabulation of (5) have been taken from 0 to 0.80. Since the values are not large it is convenient to write (5) in the form

$$G(\rho) = \frac{1}{2} \sqrt{(\pi)} e^{-\frac{1}{4}i\pi} e^{\frac{1}{4}i\pi\rho^2} - A(\rho),$$
(7)

where

$$A(\rho) = e^{\frac{1}{2}i\pi\rho^2} \int_0^{\sqrt{(\frac{1}{2}\pi)\rho}} e^{-i\lambda^2} d\lambda.$$
(8)

For several particular values of $\arg \rho$, $A(\rho)$ is expressible in terms of standard functions. Thus, in addition to the case where ρ is real, we may note that

$$A(\sigma e^{-\frac{1}{4}i\pi}) = e^{-\frac{1}{4}i\pi} e^{\frac{1}{4}\pi\sigma^2} \int_0^{\sqrt{(\frac{1}{4}\pi)\sigma}} e^{-\lambda^2} d\lambda, \qquad (9)$$

$$A(\sigma e^{\frac{1}{4}i\pi}) = e^{\frac{1}{4}i\pi} e^{-\frac{1}{2}\pi\sigma^2} \int_0^{\sqrt{(\frac{1}{2}\pi)\sigma}} e^{\lambda^2} d\lambda.$$
(10)

and

4. The method of computation

The table given is concerned with values of $|\rho|$ which are small or moderate, and the function was therefore expressed in the form (7). $A(\rho)$ was obtained from the expansion

$$e^{-\frac{1}{2}i\pi\rho^2}A(\rho) = \sum_{n=0}^{\infty} \frac{(-i)^n}{n!\,(2n+1)} \{\sqrt{(\frac{1}{2}\pi)}\,\rho\}^{2n+1}.$$
(11)

ON THE COMPLEX VALUES OF ρ 191

Since $\exp\left(\frac{1}{2}i\pi\rho^2\right)$ must be calculated in order to obtain the first term in (7), the series (11) was adopted in preference to the corresponding series for $A(\rho)$ itself, being just the more rapidly convergent of the two.

Writing $\rho = \sigma e^{i\alpha}$, pivotal values of the real and imaginary parts of (7) were obtained for values of σ from -0.2 to +1.0 at intervals of 0.1, and for values of α from -10° to $+55^{\circ}$ at intervals of 5°. These pivotal values were calculated nominally to six decimal places, up to eleven terms of (11) being taken.

They were then checked by differencing, first in the σ direction and secondly in the α direction. Differencing, however, does not detect a systematic error, or a small error at the limits of a table, and it was decided to check, by an independent calculation, the values of $G(\rho)$ for $\alpha = 0^{\circ}$, 45° for all values of σ . The formulae used were:

(a) for $\alpha = 0^{\circ}$

$$\mathscr{R}G(\rho) = \sqrt{(\frac{1}{2}\pi)} \left[\frac{1}{2} (\sin\frac{1}{2}\pi\sigma^2 + \cos\frac{1}{2}\pi\sigma^2) - \sin\frac{1}{2}\pi\sigma^2 \int_0^\sigma \sin\frac{1}{2}\pi t^2 dt - \cos\frac{1}{2}\pi\sigma^2 \int_0^\sigma \cos\frac{1}{2}\pi t^2 dt \right],$$

$$\mathscr{I}G(\rho) = \sqrt{(\frac{1}{2}\pi)} \left[\frac{1}{2} (\sin\frac{1}{2}\pi\sigma^2 - \cos\frac{1}{2}\pi\sigma^2) - \sin\frac{1}{2}\pi\sigma^2 \int_0^\sigma \cos\frac{1}{2}\pi t^2 dt + \cos\frac{1}{2}\pi\sigma^2 \int_0^\sigma \sin\frac{1}{2}\pi t^2 dt \right];$$

(b) for $\alpha = 45^{\circ}$

$$\mathscr{R}G(\rho) = e^{-\frac{1}{2}\pi\sigma^{2}} \sqrt{(\frac{1}{2}\pi)} \left[\frac{1}{2} - \frac{1}{\sqrt{2}} \int_{0}^{\sigma} e^{\frac{1}{2}\pi t^{2}} dt \right],$$

$$\mathscr{I}G(\rho) - = e^{-\frac{1}{2}\pi\sigma^{2}} \sqrt{(\frac{1}{2}\pi)} \left[\frac{1}{2} + \frac{1}{\sqrt{2}} \int_{0}^{\sigma} e^{\frac{1}{2}\pi t^{2}} dt \right].$$

A check, using formulae based on the U-series for Lommel's functions (Watson 1922, p. 545), was also made for $\alpha = -10^{\circ}$, -5° , $+40^{\circ}$, $+50^{\circ}$ for $\sigma = -0.20$, -0.10, +0.80, +0.90, +1.00.

The differencing of the pivotal values was done on a National machine and five decimal places were kept. The set of differences with respect to α was used for subtabulation of the table to every degree of the argument. This was also done on a National machine using the method described by Comrie (1936, p. 104; 1932, p. 538). A second subtabulation in the σ direction was then performed in order to produce a final table to four decimal places at interval 0.01 in $|\rho|$. Five decimals were kept throughout up to the final stage of subtabulation, together with the requisite number of fictitious figures necessary to produce an exact check at the pivotal values.

5. Applications

Since the earliest occurrence of Fresnel integrals in classical diffraction theory a number of other applications have arisen. A notable group of problems involving functions like (5) with, in general, complex values of ρ , is that for which wave propagation takes place over the surface of separation of different media. Some of these examples have been discussed by Ott (1943).

The function (5) appears frequently in wave theory for the following reason. Many problems in wave propagation may be solved by expressing the field as an angular spectrum

192 P. C. CLEMMOW AND CARA M. MUNFORD

of plane waves (Booker & Clemmow 1950), and this representation leads to solutions in the form $\int_{-\infty}^{\infty} f(x) e^{-kx^2} dx$ (10)

$$\int_{-\infty}^{\infty} f(\lambda) \,\mathrm{e}^{-k\lambda^2} \,d\lambda,\tag{12}$$

where k is real and large compared to 1. When $f(\lambda)$ has simple poles it may be shown that (12) can be reduced to a function like (5) by using a modification of the method of integration by steepest descents (Pauli 1938; Ott 1943; Clemmow 1950); the argument of this function will be complex unless the poles of $f(\lambda)$ happen to lie on the imaginary axis.

6. Other tables

In view of their many applications, the paucity of tables of Fresnel and allied integrals is disappointing (see Fletcher, Miller & Rosenhead 1946, p. 296). Even the Fresnel integrals for real values of the argument have received inadequate attention. In a recent exposition of rocket ballistics, Rankin (1949) introduced the function (5) multiplied by $\sqrt{(2/\pi)}$, and, for real values of ρ , found it necessary to compute a new table in order to obtain four figure accuracy with linear interpolation. Miller & Gordon (1931) give a lengthy discussion of some relevance which includes a valuable table of the integral (10) for real values of $x = \sqrt{(\frac{1}{2}\pi)\sigma}$, but for general complex values of the argument nothing is available; although the present table fills the gap to some extent, much yet remains to be done in this direction.

7. Description of the table

The real and imaginary parts of the function

$$G(
ho) = \sqrt{(rac{1}{2}\pi)} \, \mathrm{e}^{rac{1}{2}i\pi
ho^2} \! \int_{
ho}^{\infty} \! \mathrm{e}^{-rac{1}{2}i\pi\lambda^2} \, d\lambda$$

are tabulated to four decimal places, for values of $\arg \rho$ from 0° to 45° at intervals of 1°, and for values of $|\rho|$ from 0 to 0.80 at intervals of 0.01. The table should be accurate to within one unit of the last figure.

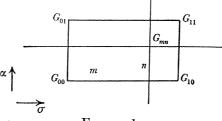
For interpolation purposes, the second differences in both directions are negligible. For interpolation in one direction only, ordinary linear interpolation in one variable can be used.

For interpolation in the two variables $\sigma = |\rho|$ and $\alpha = \arg \rho$ convenient formulae are

$$\begin{split} G_{mn} &= G_{00} + m\Delta\sigma G_{00} + n\Delta\alpha G_{00} + mn(\Delta\sigma G_{01} - \Delta\sigma G_{00}) \\ &= G_{00} + m\Delta\sigma G_{00} + n\Delta\alpha G_{00} + mn(\Delta\alpha G_{10} - \Delta\alpha G_{00}), \\ \Delta\sigma G_{00} &= G_{10} - G_{00}, \quad \Delta\alpha G_{00} = G_{01} - G_{00}, \\ \Delta\sigma G_{01} &= G_{11} - G_{01}, \quad \Delta\alpha G_{10} = G_{11} - G_{10}, \end{split}$$

where

and *m*, *n* are the fractions of the interval in the σ and α directions respectively for which the interpolated value is required (see figure 1).



ON THE COMPLEX VALUES OF ρ

These formulae are equivalent to interpolating linearly in the α -direction between G_{00} and G_{01} , and between G_{10} and G_{11} , and then in the σ -direction between the resulting G_{0n} and G_{1n} to obtain G_{mn} . They are correct at all four points (m, n) = (0, 0), (0, 1), (1, 0) and (1, 1), not only at three of these points as a formula linear in m and in n would be. A check is provided by use of the formula

$$\begin{split} G_{mn} &= G_{11} - (1-m) \, \Delta \sigma G_{01} - (1-n) \, \Delta \alpha G_{10} - (1-m) \, (1-n) \, (\Delta \alpha G_{00} - \Delta \alpha G_{10}) \\ &= G_{11} - (1-m) \, \Delta \sigma G_{01} - (1-n) \, \Delta \alpha G_{10} - (1-m) \, (1-n) \, (\Delta \sigma G_{00} - \Delta \sigma G_{01}). \end{split}$$

References

Booker, H. G. & Clemmow, P. C. 1950 Proc. Instn. Elect. Engrs., 97 Pt. III, 11.

Clemmow, P. C. 1950 Quart. J. Mech. Appl. Math. 3, 241.

Comrie, L. J. 1932 Mon. Not. R. Astr. Soc. 92, 523.

Comrie, L. J. 1936 J. Roy. Statist. Soc. Suppl. 3, 87.

- Fletcher, A., Miller, J. C. P. & Rosenhead, L. 1946 An index of mathematical tables. London: Scientific Computing Service Ltd.
- Miller, W. L. & Gordon, A. R. 1931 J. Phys. Chem. 4, 2785.

Ott, H. 1943 Ann. Phys., Lpz., 43, 393.

Pauli, W. 1938 Phys. Rev. 54, 924.

Rankin, R. A. 1949 Phil. Trans. A, 241, 457.

Watson, G. N. 1922 Theory of Bessel functions. Cambridge University Press.

PHILOSOPHICAL THE ROYAL MATHEMATICAL TRANSACTIONS SOCIETY & BENGINEERING

			194	P. C.	CLEMMO	OW AND (CARA M.	MUNFORI)		
IEERING S		4 °	$\begin{array}{c} - \ 0.6267 \\ .6274 \\ .6280 \\ .6280 \\ .6283 \\ .6285 \end{array}$	$\begin{array}{c} - \ 0.6284 \\ . 6282 \\ . 6282 \\ . 6278 \\ . 6272 \\ . 6264 \end{array}$	$\begin{array}{c} - \ 0.6255 \\ . \ 6244 \\ . \ 6232 \\ . \ 6219 \\ . \ 6204 \end{array}$	$\begin{array}{c} -0.6188 \\ \cdot 6171 \\ \cdot 6171 \\ \cdot 6152 \\ \cdot 6133 \\ \cdot 6112 \end{array}$		$\begin{array}{c} - 0.5969 \\ .5942 \\ .5914 \\ .5886 \\ .5858 \end{array}$	- 0.5828 5799 57788 5737 5737	- 0.5675 .5643 .5643 .5510 .5545	-0.5512
& ENGINEERING		3°	- 0.6267 -6272 -6276 -6276 -6277 -6276	- 0.6274 -6270 -6264 -6266 -6256	- 0.6236 -6224 -6211 -6196 -6180	-0-6162 -6144 -6124 -6123 -6103 -6081	$\begin{array}{c} -0.6059\\ \cdot 6035\\ \cdot 6011\\ \cdot 5985\\ \cdot 5959\end{array}$	$\begin{array}{c} -0.5933\\ \cdot 5905\\ \cdot 5877\\ \cdot 5848\\ \cdot 5819\\ \cdot 5819\end{array}$	- 0-5789 -5759 -5728 -5697 -5665	-0.5633 .5601 .5569 .5536 .5536	-0.5469
SOCIETY 1	$\mathscr{I}G(\rho)$	$\boldsymbol{r}^{\circ}_{\circ}$	- 0.6267 -6270 -6271 -6271 -6268	- 0.6264 .6258 .6250 .6241 .6230	$\begin{array}{c} - \ 0.6218 \\ .6204 \\ .6189 \\ .6173 \\ .6155 \end{array}$	- 0.6137 -6117 -6096 -6096 -6074 -6051	$\begin{array}{c} - \ 0.6028 \\ .6003 \\ .5978 \\ .5951 \\ .5925 \end{array}$	- 0.5897 .5869 .5840 .5811 .5811	- 0.5751 .5720 .5689 .5657 .5625	- 0.5593 .5560 .5527 .5494 .5461	-0.5427
		° —	- 0.6267 .6268 .6267 .6264 .6264	- 0.6254 .6246 .6236 .6225 .6213	$\begin{array}{c} - 0.6199 \\ \cdot 6184 \\ \cdot 6167 \\ \cdot 6150 \\ \cdot 6131 \end{array}$	- 0.6111 .6090 .6068 .6045 .6021	- 0.5997 .5971 .5945 .5918 .5890	- 0.5862 .5833 .5833 .5804 .5774 .5743	- 0.5712 .5681 .5649 .5617 .5585	- 0.5553 - 5520 - 5487 - 5487 - 5420	-0.5386
Contractions OF		°O	- 0-6267 - 6266 - 6263 - 6258 - 6252	- 0.6244 - 6234 - 6223 - 6210 - 6196	-0.6181 .6164 .6146 .6127 .6107	- 0-6086 -6063 -6040 -6016 -5991	- 0-5966 -5939 -5912 -5884 -5856	- 0-5827 -5797 -5767 -5737 -5706	- 0-5675 -5643 -5611 -5518 -5546	$\begin{array}{c} -0.6513\\ .5480\\ .5446\\ .5446\\ .5413\\ .5379\end{array}$	-0.5345
		۰ 4	+ 0.6267 -6142 -6020 -5899 -5780	+0.5663 .5547 .5547 .547 .5211 .5211	+ 0.5102 -4995 -4890 -4786 -4786 -4685	+ 0.4585 -4486 -4390 -4295 -4202	+ 0.4110 -4020 -3932 -3845 -3760	+ 0.3677 $\cdot 3595$ $\cdot 3515$ $\cdot 3436$ $\cdot 3436$ $\cdot 3359$	+ 0.3283 .3209 .3136 .3065 .2995	+ 0-2927 -2860 -2794 -2730 -2730	+0.2605
ENGINEERING		ů	$+ \begin{array}{c} 0.6267 \\ .6142 \\ .6020 \\ .5899 \\ .5780 \end{array}$	+ 0.5663 .5547 .5434 .5434 .5212 .5212	+ 0.5104 .4997 .4893 .4790 .4689	+ 0.4589 -4492 -4396 -4301 -4209	+ 0-4118 -4029 -3941 -3855 -3771	+ 0.3689 .3607 .3528 .3450 .374	+0.3299 -3225 -3153 -3083 -3083	+0.2946 -280 -2815 -2752 -2689	+0.2628
Sciel Sciel	$\mathscr{R}G(ho)$	°	+0.6267 .6142 .6020 .5899 .5780	+0.5663 .5548 .5435 .5323 .5214	+ 0-5106 -5000 -4896 -4793 -4693	+ 0.4594 -4497 -4402 -4402 -4308 -4216	+0-4126 -4038 -3951 -3866 -3782	+ 0.3700 .3620 .3541 .3464 .3389	+0.3315 -3242 -3171 -3171 -3101 -3033	+ 0-2966 -2900 -2836 -2773 -2773 -2712	+0.2652
SOCIETY	02	1	+ 0.6267 -6142 -6020 -5899 -5781	+ 0.5664 .5549 .5436 .5436 .5325 .5216	+ 0-5108 -5003 -4899 -4797 -4697	+ 0.4599 \cdot 4503 \cdot 4408 \cdot 4408 \cdot 4215 \cdot 4224	+ 0-4135 -4047 -3961 -3877 -3794	+ 0.3713 .3633 .3555 .3555 .3404	+0.3331 $\cdot 3259$ $\cdot 3188$ $\cdot 3120$ $\cdot 3052$	+ 0-2986 -2921 -2858 -2796 -2735	+0.2675
		° 0	+ 0.6267 -6142 -6020 -5899 -5781	+ 0.5664 .5550 .5437 .5327 .5218	+ 0.5111 $\cdot 5006$ $\cdot 4903$ $\cdot 4802$ $\cdot 4702$	$\begin{array}{c} + \ 0.4605 \\ \cdot 4509 \\ \cdot 4415 \\ \cdot 4323 \\ \cdot 4232 \end{array}$	+ 0.4144 .4057 .3971 .3888 .3806	+ 0.3725 .3647 .3569 .3424 .3420	+ 0.3347 -3276 -3206 -3138 -3138 -3071	+ 0.3006 $\cdot 2942$ $\cdot 2879$ $\cdot 2818$ $\cdot 2758$	+0.2699
RANSACTIONS		$\left \rho\right ^{\operatorname{arg}}$	0-0 00 03 02 04 04	0-05 -06 -03 -09 -09	0.10 .11 .12 .13 .14	0.15 .16 .17 .18 .19	0:20 :21 :22 :23 :23	0:25 :26 :27 :28 :29	0:30 :31 :32 :33 :33 :34	0:35 :36 :37 :38 :39	0.40

Downloaded from rsta.royalsocietypublishing.org

TRANSACTIONS CONTINUE & BIGINEERING

TRANSACTIONS COLLETY & MATHEMATICAL

					ON THE	COMPLEY	K VALUES	ΟF ρ		195	
SICAL NGINEERING ENCES	×.	4°	- 0.5512 .5478 .5445 .5445 .5377	$\begin{array}{c} -0.5343\\ \cdot 5308\\ \cdot 5208\\ \cdot 5240\\ \cdot 5205\end{array}$	$\begin{array}{c} -0.5171\\ \cdot 5136\\ \cdot 5136\\ \cdot 5101\\ \cdot 5067\\ \cdot 5032\end{array}$	$\begin{array}{c} -0.4998\\ \cdot4963\\ \cdot4929\\ \cdot4824\\ \cdot4894\\ \cdot4860\\ \cdot\end{array}$	$\begin{array}{c} -0.4826\\ \cdot 4792\\ \cdot 4758\\ \cdot 4758\\ \cdot 4724\\ \cdot 4691\end{array}$	$\begin{array}{c} -0.4657\\ \cdot4624\\ \cdot4591\\ \cdot4591\\ \cdot4558\\ \cdot4525\end{array}$	$\begin{array}{c} -0.4492\\ \cdot 4460\\ \cdot 4427\\ \cdot 4395\\ \cdot 4363\\ \cdot 4363\end{array}$	$\begin{array}{c} -0.4332\\ \cdot4300\\ \cdot4269\\ \cdot4269\\ \cdot4238\\ \cdot4207\\ \cdot4207\end{array}$	-0.4176
PHYS & EN & EN SCIEI		ŝ	0.5469 .5436 .5402 .5368 .5334	$\begin{array}{c} -0.5300\\ \cdot 5266\\ \cdot 5231\\ \cdot 5197\\ \cdot 5162\\ \cdot 5162\end{array}$	$\begin{array}{c} -0.5128\\ \cdot 5093\\ \cdot 5059\\ \cdot 5025\\ \cdot 4990\end{array}$	-0-4956 -4922 -4887 -4887 -4853 -4819	-0-4785 -4752 -4718 -4651 -4651	0-4618 -4585 -4582 -4519 -4487	-0-4454 -4422 -4390 -4359 -4327	- 0.4296 .4265 .4234 .4203 .4172	-0.4142
CIETY	$\mathscr{I}G(ho)$	5 °	-0.5427 .5394 .5360 .5326 .5326	$\begin{array}{c} -0.5258\\ .5223\\ .5189\\ .5155\\ .5120\\ \end{array}$	-0.5086 .5052 .5017 .4983 .4949		-0.4745 $\cdot4712$ $\cdot4678$ $\cdot4678$ $\cdot4645$ $\cdot4612$	- 0.4579 .4546 .4514 .4481 .4449		-0.4260 $\cdot4229$ $\cdot4199$ $\cdot4138$ $\cdot4138$	-0.4108
rions so		1	$\begin{array}{c} -0.5386\\ \cdot 5352\\ \cdot 5318\\ \cdot 5318\\ \cdot 5284\\ \cdot 5250\end{array}$	-0-5216 -5181 -5147 -5113 -5113	-0.5044 .5010 .4976 .4942 .4908	- 0-4874 -4840 -4806 -4772 -4739	$\begin{array}{c} -0.4705\\ -4672\\ -4639\\ -4606\\ -4573\end{array}$	- 0-4540 -4508 -4476 -4444 -4444	- 0-4380 -4349 -4317 -4286 -4286	-0.4225 -4194 -4164 -4164 -4134 -4104	-0.4075
TRANSACTIONS		° 0	$\begin{array}{c} -0.5345\\ \cdot 5311\\ \cdot 5277\\ \cdot 5277\\ \cdot 5243\\ \cdot 5209\end{array}$	$\begin{array}{c} - \ 0.5175 \\ .5140 \\ .5106 \\ .5072 \\ .5038 \end{array}$	- 0.5003 .4969 .4935 .4901 .4867	- 0.4833 -4800 -4766 -4732 -4699	- 0-4666 -4633 -4600 -4567 -4587	- 0-4502 -4470 -4438 -4406 -4375	- 0-4343 -4312 -4281 -4250 -4220	$\begin{array}{c} - \ 0.4190 \\ \cdot 4160 \\ \cdot 4130 \\ \cdot 4130 \\ \cdot 4100 \\ \cdot 4071 \end{array}$	-0.4042
		4	+ 0.2605 .2545 .2486 .2428 .2428 .2371	+ 0-2316 -2262 -2209 -2157 -2106	+0.2056 -2008 -1960 -1914 -1868	+0.1824 .1781 .1738 .1697 .1656	+0.1617 .1578 .1540 .1540 .1503 .1467	+0.1431 .1397 .1363 .1363 .1330 .1298	+ 0.1267 $\cdot 1236$ $\cdot 1236$ $\cdot 1177$ $\cdot 1148$	+0.1120 $\cdot 1093$ $\cdot 1066$ $\cdot 1040$ $\cdot 1015$	+0.0990
PHYSICAL & ENGINEERING SCIENCES		3°	+0.2628 -2569 -2510 -2413 -2397	+0.2343 -2289 -2237 -2186 -2135	+0.2086 $\cdot2038$ $\cdot1992$ $\cdot1946$ $\cdot1901$	+ 0.1857 -1814 $\cdot 1772$ $\cdot 1772$ $\cdot 1731$ $\cdot 1731$	+0.1652 -1614 -1576 -1576 -1576 -1504	+0.1469 $\cdot 1435$ $\cdot 1402$ $\cdot 1369$ $\cdot 1337$	+ 0-1306 -1276 -1246 -1246 -1217 -1189	+0.1161 -1134 -1108 -1082 -1057	+0.1032
TYA	$\mathscr{R} G(\rho)$	3 °	+0.2652 -2593 -25935 -2479 -2424	+0.2370 -2317 -2265 -2214 -2165	+ 0.2117 -2069 -2023 -1978 -1933	+0.1890 $\cdot 1848$ $\cdot 1806$ $\cdot 1766$ $\cdot 1726$	+0.1687 $\cdot 1650$ $\cdot 1613$ $\cdot 1516$ $\cdot 1541$	+ 0.1507 $\cdot 1473$ $\cdot 1440$ $\cdot 1440$ $\cdot 1408$ $\cdot 1376$	+0.1346 $\cdot 1315$ $\cdot 1286$ $\cdot 1257$ $\cdot 1229$	+ 0.1202 $\cdot 1175$ $\cdot 1149$ $\cdot 1123$ $\cdot 1098$	+0.1074
SOCIET		1°	+ 0-2675 -2617 -2560 -2504 -2504	+ 0-2396 -2344 -2293 -2293 -2243 -2194	+ 0.2146 -2100 -2054 -2009 -1965	+0.1923 $\cdot 1881$ $\cdot 1840$ $\cdot 1840$ $\cdot 1761$	+ 0.1723 + 0.1723 - 0.1685 - 0.1649 - 0.1649 - 0.1613 - 0.1578 - 0.1588 -	+0.1544 -1510 -1478 -1478 -1446 -1415	+0.1384 $\cdot1355$ $\cdot1325$ $\cdot1325$ $\cdot1297$ $\cdot1269$	+0.1242 .1216 .1190 .1164 .1139	+0.1115
		°0° d	+ 0.2699 -2641 -2585 -2585 -2530 -2476	+ 0.2423 -2372 -2321 -2272 -2224	+ 0.2176 -2130 -2085 -2041 -1997	+ 0.1955 $\cdot 1914$ $\cdot 1873$ $\cdot 1834$ $\cdot 1795$	+ 0.1757 - 1720 - 1684 - 1649 - 1614	$\begin{array}{c} + \ 0.1581 \\ \cdot 1548 \\ \cdot 1515 \\ \cdot 1484 \\ \cdot 1453 \\ \cdot 1453 \end{array}$	+ 0.1423 $\cdot 1393$ $\cdot 1364$ $\cdot 1364$ $\cdot 1309$	+ 0.1282 $\cdot 1255$ $\cdot 1230$ $\cdot 1205$ $\cdot 1180$	+0.1156
TRANS		$\left \rho\right $	0-40 -41 -42 -43 -44	0:45 :46 :47 :48 :49	0 51 53 53 54	0 55 57 53 59 59	0-60 61 63 64	0-65 -66 -67 -68 -69	0.70 .71 .72 .73 .73	0-75 -77 -77 -78 -78 -79	0.80

THE ROYAL MATHEMATICAL THE ROYAL MATHEMATICAL

PHILOSOPHICAL THE ROYAL A MATHEMATICAL,

		196	P. C	. CLEMM	OW AND	CARA M.	MUNFOR	D		
0	° 6	- 0.6267 -6285 -6301 -6315 -6315 -6326	- 0.6335 - 0.6332 - 6342 - 6347 - 6350 - 6351	0.6350 	-0.6320 $\cdot 6309$ $\cdot 6297$ $\cdot 6283$ $\cdot 6283$	-0.6252 .6234 .6216 .6116 .6175	-0.6153 $\cdot 6130$ $\cdot 6130$ $\cdot 6082$ $\cdot 6056$	- 0.6030 -6003 -5975 -5947 -5917	- 0.5888 -5857 -5827 -5827 -5795 -5763	-0.5731
	õo	-0.6267 .6283 .6297 .6308 .6318	- 0.6325 .6330 .6333 .6333 .6334 .6334	-0.6331 -6327 -6321 -6321 -6313 -6304	-0-6293 -6281 -6267 -6253 -6233	$\begin{array}{c} -0.6219\\ .6200\\ .6181\\ .6180\\ .6138\\ .6138\end{array}$	-0.6116 .6092 .6067 .6042 .6016	-0.5989 .5961 .5933 .5933 .5904 .5874	- 0.5844 .5813 .5751 .5751 .5719	-0.5686
$\mathcal{I} G(\rho)$	7 °	-0.6267 .6281 .6292 .6302 .6309	$\begin{array}{c} -0.6315\\ \cdot6318\\ \cdot6319\\ \cdot6319\\ \cdot6319\\ \cdot6316\\ \cdot6316\end{array}$	-0.6312 -6306 -6298 -6298 -6279	- 0-6267 -6253 -6238 -6238 -6222	$\begin{array}{c} -0.6187\\ \cdot 6167\\ \cdot 6146\\ \cdot 6125\\ \cdot 6102\end{array}$	$\begin{array}{c} -0.6078\\ \cdot 6054\\ \cdot 6029\\ \cdot 6002\\ \cdot 5976\end{array}$	$\begin{array}{c} -0.5948\\ \cdot 5920\\ \cdot 5891\\ \cdot 5891\\ \cdot 5831\\ \cdot 5831\end{array}$	- 0.5801 .5770 .5778 .5738 .5707 .5674	-0.5642
	9	-0.6267 -6279 -6278 -6288 -6296 -6301	-0.6304 -6306 -6305 -6303 -6303 -6299	- 0.6293 .6285 .6276 .6276 .6266 .6254	-0.6240 -0.6226 -6209 -6192 -6174	- 0.6154 .6134 .6112 .6089 .6066	- 0.6041 .6016 .5990 .5963 .5936	- 0-5908 -5879 -5850 -5820 -5789	- 0-5758 -5727 -5695 -5663 -5631	-0.5598
5	ũ	- 0.6267 .6276 .6284 .6289 .6293		- 0-6274 -6265 -6265 -6254 -6229	- 0.6214 .6198 .6181 .6162 .6143	$\begin{array}{c} - \ 0.6122 \\ \cdot \ 6100 \\ \cdot \ 6078 \\ \cdot \ 6054 \\ \cdot \ 6030 \end{array}$	$\begin{array}{c} - 0.6005 \\ \cdot 5979 \\ \cdot 5952 \\ \cdot 5925 \\ \cdot 5897 \\ \cdot 5897 \end{array}$	- 0.5868 .5839 .5839 .5809 .5778 .5748	- 0.5716 .5685 .5685 .5653 .5620 .5587	-0.5554
	°6	+0.6267 -6143 -6022 -5901 -5782	+ 0.5664 .5548 .5433 .5319 .5207	+ 0.5097 .4988 .4880 .4774 .4670	+ 0-4567 - 4466 - 4466 - 4366 - 4366 - 4171	+0.4076 $\cdot3982$ $\cdot3890$ $\cdot3890$ $\cdot3711$	+ 0.3624 .3538 .3538 .35453 .3711 .3289	+0.3209 $\cdot3131$ $\cdot3054$ $\cdot2979$ $\cdot2905$	+0.2832 -2761 -2691 -2623 -2556	+0.2490
IENCES	õ	+0.6267 -6143 -6021 -5900 -5781	+0.5664 .5547 .5432 .5432 .5319 .5207	+ 0.5097 .4989 .4882 .4776 .4672	+0-4570 -4469 -4370 -4272 -4176	+0.4082 $\cdot 3989$ $\cdot 3898$ $\cdot 3898$ $\cdot 3808$ $\cdot 3720$	+0-3633 -3548 -3465 -3465 -3363 -3383 -3302	+ 0.3224 .3146 .3070 .2995 .2922	+0.2851 -2780 -2711 -2644 -2578	+0.2513
$\mathscr{R} G(\rho)$	1 °	+0.6267 .6143 .6021 .5900 .5781	+0.5663 .5547 .5432 .5319 .5208	+ 0.5098 .4990 .4883 .4778 .4675	+ 0-4573 -4473 -4374 -4278 -4182	+0-4089 -3996 -3906 -3817 -3817	+0.3644 .3560 .3477 .3396 .3316	+0-3238 -3161 -3086 -3086 -3012 -2940	+0.2869 -2800 -2732 -2600 -2600	+0.2536
	° 9	+0-6267 -6143 -6020 -5900 -5780	$\begin{array}{c} + \ 0.5663 \\ \cdot 5547 \\ \cdot 5432 \\ \cdot 5432 \\ \cdot 5320 \\ \cdot 5209 \end{array}$	+ 0.5099 -4991 -4885 -4781 -4781	+ 0.4577 $\cdot 4477$ $\cdot 4379$ $\cdot 4283$ $\cdot 4188$	+0-4095 -4004 -3914 -3826 -3739	+0.3654 .3571 .3489 .3409 .3330	+ 0-3253 -3177 -3103 -3103 -3030 -2958	+0.2888 -2820 -2752 -2752 -2686 -2622	+0.2559
) .	<i>b</i>	+ 0.6267 -6143 -6020 -5899 -5780	+0.5663 .5547 .5433 .5433 .5320 .5209	+ 0-5100 -4993 -4887 -4887 -4783 -4783 -4681	+0.4580 $\cdot4482$ $\cdot4384$ $\cdot4384$ $\cdot4289$ $\cdot4195$	+0.4103 -4012 -3923 -3835 -3750	+0.3665 .3583 .3502 .3422 .3344	+ 0-3268 -3193 -3119 -3047 -2977	+ 0.2907 -2840 -2773 -2773 -2708 -2644	+0.2582
5	$\left \rho\right $	0.00 01 03 •04	0.05 06 07 08 09	0·10 ·11 ·12 ·13 ·14	0.15 .16 .17 .18 .19	0-20 -21 -23 -24	0:25 .26 .28 .28 .29	0:30 31 32 33 34	0:35 :36 :37 :38 :39	0.40

Downloaded from rsta.royalsocietypublishing.org

PHILOSOPHICAL THE ROYAL MATHEMATICAL, TRANSACTIONS SOCIETY Sciences

PHILOSOPHICAL THE ROYAL MATHEMATICAL, TRANSACTIONS SOCIETY Sciences

IRAN							•				
PHILOSOPHICAL FRANSACTIONS		$ \rho $	040 41 43 43 44	0 46 47 48 49	0 51 53 53 54 53	0 55 57 58 58 59	0.60 61 63 63 63	0 66 69 69 69 69	0.70 .71 .72 .73	0.75 .76 .77 .78 .79	0.80
THE		о <mark>л</mark> о	+ 0.2582 $\cdot 2521$ $\cdot 2461$ $\cdot 2402$ $\cdot 2345$	+ 0.2289 $\cdot 2234$ $\cdot 2180$ $\cdot 2128$ $\cdot 2128$ $\cdot 2076$	+ 0.2026 $\cdot 1977$ $\cdot 1929$ $\cdot 1882$ $\cdot 1836$	+ 0.1791 $\cdot 1747$ $\cdot 1704$ $\cdot 1662$ $\cdot 1621$	$\begin{array}{c} + \ 0.1581 \\ \cdot 1541 \\ \cdot 1503 \\ \cdot 1503 \\ \cdot 1466 \\ \cdot 1429 \end{array}$	+ 0.1393 $\cdot 1358$ $\cdot 1324$ $\cdot 1291$ $\cdot 1258$	+ 0.1227 $\cdot 1196$ $\cdot 1165$ $\cdot 1136$ $\cdot 1107$	+ 0.1078 $\cdot 1051$ $\cdot 1024$ $\cdot 0998$ $\cdot 0972$	+0.0947
ROYAL IETY	č	°9	+0.2559 -2497 -2436 -2436 -2377 -2319	+ 0.2262 -2207 -2152 -2099 -2047	+0.1996 $\cdot 1946$ $\cdot 1897$ $\cdot 1850$ $\cdot 1803$	+0.1757 $\cdot 1713$ $\cdot 1669$ $\cdot 1627$ $\cdot 1585$	+ 0.1545 -1505 -1466 -1428 -1391	+ 0.1355 $\cdot 1320$ $\cdot 1285$ $\cdot 1218$ $\cdot 1218$	+ 0.1186 -1155 -1124 -1094 -1065	+0.1036 $\cdot 1008$ $\cdot 0981$ $\cdot 0929$	+0.0904
	$\mathscr{R} G(\rho)$	7°	+0.2536 $\cdot 2473$ $\cdot 2412$ $\cdot 2352$ $\cdot 2352$	+ 0.2235 -2179 -2124 -2124 -2070 -2017	+0.1966 $\cdot 1915$ $\cdot 1816$ $\cdot 1817$ $\cdot 1770$	+0.1724 $\cdot 1679$ $\cdot 1635$ $\cdot 1592$ $\cdot 1549$	+0.1508 -1468 -1429 -1390 -1353	+0.1316 -1280 -1245 -1245 -1211 -1178	+ 0.1145 $\cdot 1114$ $\cdot 1082$ $\cdot 1052$ $\cdot 1023$	+0.0994 0.0966 0.038 0.0311 0.0911	+0.0860
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		ŝ	+ 0.2513 -2450 -23450 -2387 -2327 -2267	+0.2209 -2151 -2096 -2041 -1987	+0.1935 .1884 .1884 .1785 .1785	+0.1690 $\cdot 1644$ $\cdot 1600$ $\cdot 1556$ $\cdot 1513$	+0.1472 $\cdot 1431$ $\cdot 1391$ $\cdot 1352$ $\cdot 1314$	+ 0.1277 + 0.1241 - 0.1241 - 0.1205 - 0.1205 - 0.1137 - 0.01137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.1137 - 0.0137 - 0.0137 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0	+ 0.1104 $\cdot 1072$ $\cdot 1040$ $\cdot 1040$ $\cdot 1010$ $\cdot 0980$	+ 0.0951 $\cdot 0922$ $\cdot 0894$ $\cdot 0867$ $\cdot 0841$	+0.0815
TRA		° 6	+ 0-2490 -2426 -2363 -2363 -2301 -2241	+ 0-2182 -2124 -2067 -2067 -1958	+0.1905 -1853 -1862 -1752 -1704	+0.1656 $\cdot 1610$ $\cdot 1565$ $\cdot 1520$ $\cdot 1477$	+0.1435 $\cdot 1393$ $\cdot 1353$ $\cdot 1353$ $\cdot 1313$ $\cdot 1275$	+0.1237 $\cdot1200$ $\cdot1165$ $\cdot1130$ $\cdot1095$	+0.1062 $\cdot 1029$ $\cdot 0.998$ $\cdot 0.998$ $\cdot 0.936$	+ 0.0907 -0878 -0850 -0850 -0850 -0796	+0.0770
PHILOSOPHICAL TRANSACTIONS		ິດ	$\begin{array}{c} - 0.5554 \\ .5521 \\ .5521 \\ .5428 \\ .5420 \\ .5420 \end{array}$	$\begin{array}{c} -0.5386\\ \cdot5352\\ \cdot5317\\ \cdot5217\\ \cdot5283\\ \cdot5248\end{array}$	$\begin{array}{c} - 0.5214 \\ .5179 \\ .51144 \\ .51110 \\ .5075 \end{array}$	$\begin{array}{c} - 0.5040 \\ .5005 \\ .4971 \\ .4936 \\ .4936 \\ .4902 \end{array}$	-0.4867 $\cdot 4833$ $\cdot 4799$ $\cdot 4765$ $\cdot 4731$	$\begin{array}{c} - 0.4697 \\ -4663 \\ -4630 \\ -4530 \\ -4597 \\ -4563 \end{array}$	$\begin{array}{c} - 0.4530 \\ \cdot 4497 \\ \cdot 4465 \\ \cdot 4465 \\ \cdot 4432 \\ \cdot 4400 \end{array}$	$\begin{array}{c} - \ 0.4368 \\ \cdot 4336 \\ \cdot 4336 \\ \cdot 4304 \\ \cdot 4273 \\ \cdot 4242 \end{array}$	-0.4211
THE ROYAL SOCIETY		°9	- 0.5598 .5565 .5531 .5498 .5464	$\begin{array}{c} -0.5430\\ \cdot5395\\ \cdot5381\\ \cdot5321\\ \cdot5292\\ \cdot5292\end{array}$	-0.5257 .5223 .5188 .5153 .5118	$\begin{array}{c} -0.5083\\ \cdot 5048\\ \cdot 5013\\ \cdot 4979\\ \cdot 4944\\ \cdot 4944\end{array}$		$\begin{array}{c} - \ 0.4737 \\ \cdot 4703 \\ \cdot 4703 \\ \cdot 4670 \\ \cdot 4636 \\ \cdot 4602 \end{array}$	0-4569 -4536 -4503 -4470 -4470	$\begin{array}{c} - 0.4405 \\ \cdot 4372 \\ \cdot 4340 \\ \cdot 4308 \\ \cdot 4207 \end{array}$	-0.4245
A TY TY	$\mathscr{I}G(\rho)$	7 °	$\begin{array}{c} - \ 0.5642 \\ .5609 \\ .5575 \\ .5542 \\ .5542 \\ .5508 \end{array}$	- 0.5474 -5440 -5440 -53406 -5371 -5336	$\begin{array}{c} - 0.5302 \\ \cdot 5267 \\ \cdot 5232 \\ \cdot 5197 \\ \cdot 5162 \end{array}$	$\begin{array}{c} - 0.5127 \\ \cdot 5092 \\ \cdot 5057 \\ \cdot 5021 \\ \cdot 4987 \end{array}$	$\begin{array}{c} -0.4952\\ \cdot4917\\ \cdot4812\\ \cdot4882\\ \cdot4847\\ \cdot4813\end{array}$	$\begin{array}{c} - \ 0.4778 \\ \cdot 4744 \\ \cdot 4710 \\ \cdot 4676 \\ \cdot 4676 \\ \cdot 4642 \end{array}$		$\begin{array}{c} - 0.4442 \\ \cdot 4409 \\ \cdot 4377 \\ \cdot 4374 \\ \cdot 4312 \\ \cdot 4312 \end{array}$	-0.4281
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		° So	- 0.5686 .5653 .5620 .5587 .5553	$\begin{array}{c} -0.5519\\ \cdot5485\\ \cdot5480\\ \cdot5450\\ \cdot5416\\ \cdot5381\end{array}$	-0.5346 .5311 .5276 .5241 .5206	$\begin{array}{c} -0.5171\\ \cdot5135\\ \cdot5136\\ \cdot5100\\ \cdot5065\\ \cdot5030\end{array}$	$\begin{array}{c} - 0.4995 \\ \cdot 4959 \\ \cdot 4959 \\ \cdot 4924 \\ \cdot 4889 \\ \cdot 4854 \end{array}$	$\begin{array}{c} -0.4820\\ \cdot4785\\ \cdot4750\\ \cdot4750\\ \cdot4716\\ \cdot4682\end{array}$	$\begin{array}{c} - \ 0.4648 \\ \cdot 4614 \\ \cdot 4580 \\ \cdot 4580 \\ \cdot 4546 \\ \cdot 4513 \end{array}$	$\begin{array}{c} - \ 0.4479 \\ \cdot 4446 \\ \cdot 4413 \\ \cdot 4413 \\ \cdot 4381 \\ \cdot 4381 \\ \cdot 4348 \end{array}$	-0.4316
IL, IG		° 6	$\begin{array}{c} - \ 0.5731 \\ \cdot 5699 \\ \cdot 5666 \\ \cdot 5632 \\ \cdot 5539 \end{array}$	$\begin{array}{c} - \ 0.5565 \\ \cdot 5531 \\ \cdot 5531 \\ \cdot 5496 \\ \cdot 5462 \\ \cdot 5427 \end{array}$	-0.5392 .5357 .5322 .5226 .5251	-0.5215 $\cdot 5180$ $\cdot 5144$ $\cdot 5109$ $\cdot 5073$	- 0.5038 .5003 .4967 .4932 .4897	$\begin{array}{c} -0.4861\\ \cdot 4826\\ \cdot 4792\\ \cdot 4757\\ \cdot 4757\\ \cdot 4722\end{array}$	$\begin{array}{c} - \ 0.4688 \\ \cdot 4653 \\ \cdot 4619 \\ \cdot 4585 \\ \cdot 4551 \end{array}$	- 0.4517 .4484 .44450 .4417 .4384	-0.4352

Vol. 245. A.

Downloaded from rsta.royalsocietypublishing.org

ON THE COMPLEX VALUES OF ρ

197

MATHEMATICAL, PHYSICAL & ENGINEERING

24

			198	P. C.	CLEMMO	OW AND (CARA M.	MUNFORI	D		
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		14 °	- 0.6267 -6296 -6322 -6346 -6367	-0.6386 -6403 -6417 -6417 -6429 -6439	$\begin{array}{c} - 0.6447 \\ .6452 \\ .6456 \\ .6456 \\ .6458 \\ .6457 \end{array}$	-0.6455 .6452 .6446 .6439 .6439 .6430	-0.6420 .6408 .6395 .6380 .6364		-0.6243 .6219 .6194 .6168 .6141	-0.6114 .6086 .6057 .6027 .5997	-0.5966
PHYSIC PHYSIC & ENGI		13 °	$\begin{array}{c} - 0.6267 \\ \cdot 6294 \\ \cdot 6318 \\ \cdot 6318 \\ \cdot 6340 \\ \cdot 6359 \end{array}$	$\begin{array}{c} -0.6376\\ \cdot 6391\\ \cdot 6391\\ \cdot 6403\\ \cdot 6413\\ \cdot 6421\end{array}$	- 0.6427 .6431 .6433 .6433 .6433	- 0.6428 .6423 .6416 .6417 .6397	- 0.6386 .6373 .6373 .6358 .6342 .6325	- 0.6307 .6288 .6288 .6246 .6223	$\begin{array}{c} - 0.6199 \\ \cdot 6175 \\ \cdot 6175 \\ \cdot 6149 \\ \cdot 6123 \\ \cdot 6095 \end{array}$	$\begin{array}{c} -0.6068\\ \cdot 6039\\ \cdot 6039\\ \cdot 5979\\ \cdot 5949\\ \cdot 5949\end{array}$	-0.5917
THE ROYAL SOCIETY	$\mathscr{I} G(\rho)$	12 °	$\begin{array}{c} -0.6267\\ \cdot 6291\\ \cdot 6314\\ \cdot 6333\\ \cdot 6333\\ \cdot 6351\end{array}$	$\begin{array}{c} -0.6366\\ \cdot6378\\ \cdot6378\\ \cdot6389\\ \cdot6397\\ \cdot6404\end{array}$	$\begin{array}{c} - 0.6408\\ \cdot 6410\\ \cdot 6410\\ \cdot 6410\\ \cdot 6409\\ \cdot 6406\end{array}$	$\begin{array}{c} - 0.6401\\ \cdot 6394\\ \cdot 6386\\ \cdot 6376\\ \cdot 6365\end{array}$	$\begin{array}{c} - 0.6352\\ \cdot 6338\\ \cdot 6338\\ \cdot 6322\\ \cdot 6305\\ \cdot 6287\end{array}$	- 0.6268 .6248 .6226 .6204 .6181	$\begin{array}{c} -0.6156\\ \cdot 6131\\ \cdot 6105\\ \cdot 6078\\ \cdot 6050\\ \cdot 6050\end{array}$	- 0.6022 .5993 .5963 .5932 .5901	-0.5870
		11 °	$\begin{array}{c} - 0.6267 \\ \cdot 6289 \\ \cdot 6309 \\ \cdot 6327 \\ \cdot 6342 \end{array}$	- 0.6356 .6366 .6375 .6381 .6381	- 0.6389 .6389 .6388 .6385 .6385	- 0.6374 .6365 .6356 .6345 .6332	$\begin{array}{c} - 0.6318 \\ \cdot 6303 \\ \cdot 6303 \\ \cdot 6286 \\ \cdot 6269 \\ \cdot 6250 \end{array}$	- 0.6229 .6208 .6186 .6163 .6139	$\begin{array}{c} - 0.6114 \\ \cdot 6088 \\ \cdot 6061 \\ \cdot 6034 \\ \cdot 6005 \end{array}$	- 0.5976 .5947 .5917 .5886 .5855	-0.5823
PHILOSOPHICAL TRANSACTIONS		10 °	- 0.6267 .6287 .6287 .6305 .6321 .6334	- 0-6345 -6354 -6361 -6366 -6366	- 0.6369 .6368 .6365 .6365 .6361	- 0.6347 .6337 .6326 .6314 .6300	- 0-6285 -6288 -6268 -6251 -6232 -6212	-0.6191 -0.6191 -6169 -6122 -6097	- 0.6072 .6045 .6018 .5990 .5961	$\begin{array}{c} - 0.5932 \\ \cdot 5902 \\ \cdot 5871 \\ \cdot 5840 \\ \cdot 5809 \end{array}$	-0.5777
		14 °	+0.6267 .6145 .6025 .5906 .5787	+0.5670 .5553 .55438 .5324 .52211	+0.5099 $\cdot4988$ $\cdot4879$ $\cdot4871$ $\cdot4771$ $\cdot4664$	+0.4558 $\cdot4454$ $\cdot4352$ $\cdot4352$ $\cdot4352$ $\cdot4150$	+0.4051 $\cdot3954$ $\cdot3858$ $\cdot3764$ $\cdot3671$	+0.3579 $\cdot 3489$ $\cdot 3401$ $\cdot 3314$ $\cdot 3228$	+0.3144 $\cdot 3061$ $\cdot 2979$ $\cdot 2821$	+ 0.2744 -2668 -2594 -2521 -2449	+0.2379
ATHEMATICAL, HYSICAL ENGINEERING CIENCES		13°	+ 0.6267 -6145 -6024 -5905 -5786	+0.5668 .5552 .5437 .5322 .5210	+ 0.5098 .4988 .4879 .4771 .4771	+0.4559 $\cdot4456$ $\cdot4354$ $\cdot4354$ $\cdot4253$ $\cdot4153$	+ 0-4056 - 3959 - 3864 - 3770 - 3678	+0.3587 .3498 .3411 .3324 .3239	+0.3156 .3074 .2994 .2915 .2837	+0-2761 -2686 -2613 -2613 -2541 -2470	+0.2401
	$\mathscr{R}G(ho)$	12 °	+0.6267 -6145 -6023 -5904 -5785	+ 0.5667 .5551 .5435 .5321 .5321	+ 0.5097 .4987 .4878 .4878 .4771	+ 0-4561 -4458 -4458 -4356 -4356 -4157	+ 0-4060 -3964 -3870 -3870 -3777 -3686	+0.3596 .3508 .3421 .3335 .3335 .3251	+0.3169 $\cdot 3088$ $\cdot 3008$ $\cdot 2930$ $\cdot 2853$	+0.2778 $\cdot 2704$ $\cdot 2632$ $\cdot 2561$ $\cdot 2491$	+0.2423
THE ROYAL SOCIETY	<i>a</i>	11 °	+ 0.6267 $\cdot 6144$ $\cdot 6023$ $\cdot 5903$ $\cdot 5784$	$\begin{array}{c} + \ 0.5666 \\ \cdot 5549 \\ \cdot 5434 \\ \cdot 5434 \\ \cdot 5320 \\ \cdot 5208 \end{array}$	+ 0.5097 $\cdot 4987$ $\cdot 4879$ $\cdot 4772$ $\cdot 4666$	+0.4563 -4460 -4359 -4359 -4259 -4161	+ 0-4065 - 3970 - 3876 - 3784 - 3694	+ 0-3605 -3517 -3431 -3347 -3347 -3264	+0.3182 $\cdot3102$ $\cdot3023$ $\cdot2946$ $\cdot2870$	+ 0-2796 -2723 -2652 -2681 -2513	+0.2445
	1	ρ 10 °	+ 0.6267 -6144 -6022 -5902 -5783	+0.5665 -5549 -5433 -5433 -5208	+ 0.5097 .4987 .4879 .4879 .4773 .4668	+0.4565 $\cdot4463$ $\cdot4463$ $\cdot4263$ $\cdot4263$ $\cdot4166$	+0.4070 $\cdot 3976$ $\cdot 3833$ $\cdot 3792$ $\cdot 3702$	+0.3614 $\cdot3527$ $\cdot3442$ $\cdot3358$ $\cdot3276$	+0.3196 $\cdot3116$ $\cdot3039$ $\cdot2962$ $\cdot2887$	+ 0.2814 -2742 -2671 -2602 -2534	+0.2468
PHILOSOPHICAL TRANSACTIONS	ŝ	$ \rho $	0-00 02 03 04 03	0-05 -06 -08 -09 -09	0:10 11 12 13 13	0:15 :16 :17 :18	0:20 21 23 23 23 24	0-25 -26 -28 -28 -28	0:30 31 33 33 33 34	0:35 36 37 38 39	0-40

SOCIETY A	
PHILOSOPHICAI TRANSACTIONS	
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES	
THE ROYAL A SOCIETY	

PHILOSOPHICAL TRANSACTIONS

MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES

							o or p		100	
	14 °	$\begin{array}{c} -0.5966\\ \cdot 5934\\ \cdot 5902\\ \cdot 5869\\ \cdot 5836\end{array}$	- 0.5803 .5769 .5734 .5700 .5665	-0.5629 .5594 .5558 .5522 .5485	-0.5449 $\cdot 5412$ $\cdot 5376$ $\cdot 5339$ $\cdot 5302$	-0.5265 .5228 .5191 .5117	- 0.5080 .5043 .5043 .5006 .4969 .4932	-0.4896 $\cdot4859$ $\cdot4859$ $\cdot4823$ $\cdot4786$ $\cdot4750$	- 0.4714 .4678 .4643 .4607 .4572	-0.4537
	13 °	-0.5917 .5886 .5853 .5821 .5821	-0.5754 -5720 -5685 -5651 -5651	- 0.5580 .5545 .5509 .5473 .5473	-0.5401 $\cdot5365$ $\cdot5328$ $\cdot5292$ $\cdot5255$	$\begin{array}{c} -0.5218\\ \cdot 5182\\ \cdot 5145\\ \cdot 5145\\ \cdot 5108\\ \cdot 5072\end{array}$	$\begin{array}{c} -0.5035\\ \cdot4998\\ \cdot4962\\ \cdot4962\\ \cdot4889\\ \cdot4889\end{array}$	$\begin{array}{c} -0.4853\\ \cdot4817\\ \cdot4817\\ \cdot4781\\ \cdot4745\\ \cdot4709\\ \cdot4709\end{array}$	$\begin{array}{c} -0.4674\\ \cdot4638\\ \cdot4638\\ \cdot4603\\ \cdot4568\\ \cdot4568\\ \cdot4533\end{array}$	-0.4499
$\mathscr{I} G(\rho)$	12 °	$\begin{array}{c} -0.5870\\ .5838\\ .5838\\ .5805\\ .5772\\ .5739\\ .5739\end{array}$	- 0.5705 -5671 -5637 -5637 -5602 -5567	$\begin{array}{c} -0.5532\\ \cdot 5497\\ \cdot 5461\\ \cdot 5425\\ \cdot 5390\end{array}$	$\begin{array}{c} -0.5354\\ \cdot5317\\ \cdot5317\\ \cdot5281\\ \cdot5245\\ \cdot5209\end{array}$	-0.5172 .5136 .5100 .5063 .5027	-0.4991 -4955 -4918 -4918 -4882 -4846	- 0-4811 -4775 -4740 -4704 -4669	- 0-4634 -4599 -4564 -4530 -4496	-0.4461
	11°	-0.5823 .5791 .5758 .5725 .5725	$\begin{array}{c} -0.5658\\ \cdot5624\\ \cdot5528\\ \cdot5555\\ \cdot5555\end{array}$	$\begin{array}{c} - \ 0.5485 \\ \cdot 5449 \\ \cdot 5414 \\ \cdot 5378 \\ \cdot 5343 \\ \cdot 5343 \end{array}$	$\begin{array}{c} -0.5307\\ \cdot5271\\ \cdot5235\\ \cdot5199\\ \cdot5163\\ \end{array}$	$\begin{array}{c} -0.5127\\ \cdot5091\\ \cdot5065\\ \cdot5019\\ \cdot4983\end{array}$	- 0-4947 - 4911 - 4816 - 4840 - 4804	- 0.4769 -4734 -4699 -4664 -4629	- 0.4595 .4560 .4526 .4492 .4458	-0.4424
	10°	-0.5777 .5744 .5712 .5678 .5645	$\begin{array}{c} - \ 0.5611 \\ .5577 \\ .5542 \\ .5508 \\ .5473 \end{array}$	$\begin{array}{c} -0.5438\\ \cdot 5403\\ \cdot 5367\\ \cdot 5332\\ \cdot 5332\\ \cdot 5296\end{array}$	$\begin{array}{c} -0.5261\\ \cdot 5225\\ \cdot 5189\\ \cdot 5154\\ \cdot 5118\end{array}$	-0.5082 .5046 .5011 .4975 .4939	-0.4904 $\cdot4869$ $\cdot4833$ $\cdot4798$ $\cdot4763$	$\begin{array}{c} -0.4728\\ \cdot 4693\\ \cdot 4659\\ \cdot 4624\\ \cdot 4520\\ \cdot 4590\end{array}$	- 0-4556 -4522 -4488 -4488 -4454 -4421	-0.4388
	14°	+0.2379 -2310 -2243 -2177 -2112	+0.2049 $\cdot 1987$ $\cdot 1926$ $\cdot 1866$ $\cdot 1808$	+0.1751 $\cdot 1695$ $\cdot 1640$ $\cdot 1587$ $\cdot 1535$	+0.1484 -1434 -1385 -1337 -1290	+0.1245 $\cdot 1200$ $\cdot 1157$ $\cdot 1115$ $\cdot 1073$	+0.1033 -0993 -0955 -0917 -0811	+0-0845 -0810 -0776 -0743 -0711	+0-0679 -0649 -0619 -0590 -0590	+0.0534
	13 °	+0.2401 -2333 -2267 -2202 -2138	+0.2075 $\cdot 2014$ $\cdot 1954$ $\cdot 1895$ $\cdot 1838$	+0.1782 $\cdot 1727$ $\cdot 1673$ $\cdot 1620$ $\cdot 1569$	+0.1518 $\cdot 1469$ $\cdot 1421$ $\cdot 1374$ $\cdot 1328$	+0.1284 $\cdot 1240$ $\cdot 1197$ $\cdot 11155$ $\cdot 1114$	+0.1075 -1036 -0998 -0961 -0925	+0.0890 -0855 -0822 -0757	+0-0726 -0696 -0666 -0638 -0610	+0.0582
$\mathscr{R}G(ho)$	12 °	+0-2423 -2356 -2291 -2226 -2163	+0.2102 $\cdot 2041$ $\cdot 1982$ $\cdot 1925$ $\cdot 1868$	+0.1813 $\cdot 1758$ $\cdot 1705$ $\cdot 1654$ $\cdot 1603$	+0.1553 -1505 -1457 -1411 -1366	+0.1322 $\cdot 1279$ $\cdot 1237$ $\cdot 1195$ $\cdot 1155$	+0.1116 $\cdot 1078$ $\cdot 1040$ $\cdot 1004$ $\cdot 0968$	+0.0934 -0900 -0867 -0834 -0833	+0.0772 -0742 -0713 -0685 -0657	+0.0630
03	•11	+0.2445 -2379 -2315 -2251 -2189	+ 0.2128 -2069 -2011 -1954 -1898	+0.1843 $\cdot 1790$ $\cdot 1738$ $\cdot 1687$ $\cdot 1637$	+0.1588 $\cdot 1540$ $\cdot 1493$ $\cdot 1448$ $\cdot 1403$	+0.1360 $\cdot 1317$ $\cdot 1276$ $\cdot 1235$ $\cdot 1195$	+0.1157 -1119 -1082 -1082 -1046 -1011	+0.0977 -0943 -0911 -0879 -0848	+0.0818 -0.788 -0.759 -0.731 -0.704	+0.0677
	ρ 10 °	+ 0-2468 -2403 -2339 -2276 -2215	+ 0.2155 -2096 -2039 -1983 -1928	+ 0.1874 -1821 -1770 -1720 -1670	+ 0.1622 $\cdot 1575$ $\cdot 1529$ $\cdot 1440$ $\cdot 1440$	+ 0.1397 $\cdot 1355$ $\cdot 1314$ $\cdot 1274$ $\cdot 1235$	+ 0.1197 -1160 -1124 -1088 -1054	+0-1020 -0987 -0955 -0923 -0892	+ 0.0863 -0833 -0805 -0777 -0750	+0.0724
	$ \rho $	040 41 42 43 44	0.45 46 47 47 48	0 51 53 54 54	0 56 57 57 59	0.60 .61 .63 .63	0.65 66 67 69 69	0.70 .71 .72 .73 .74	0.75 .76 .77 .78 .79	0.80

ON THE COMPLEX VALUES OF ρ

24-2

199

			200	P. C.	CLEMMC	OW AND C	CARA M. I	MUNFORI)		
SERING		19 °	0.6267 	- 0.6437 .6463 .6487 .6588 .6508	$\begin{array}{c} - \ 0.6544 \\ .6558 \\ .6571 \\ .6581 \\ .6581 \\ .6588 \end{array}$	- 0.6594 .6598 .6600 .6600 .6600	$\begin{array}{c} -0.6594 \\ .6588 \\ .6588 \\ .6572 \\ .6572 \\ .6561 \end{array}$	$\begin{array}{c} -0.6549\\ .6536\\ .6521\\ .6521\\ .6504\\ .6487\end{array}$		$\begin{array}{c} - \ 0.6355 \\ . 6329 \\ . 6329 \\ . 6302 \\ . 6275 \\ . 6246 \end{array}$	-0.6217
		18°	- 0.6267 -6304 -6339 -6339 -6371	- 0.6427 -6451 -6451 -6473 -6493 -6510	$\begin{array}{c} -0.6525\\ .6537\\ .6537\\ .6548\\ .6556\\ .6562\end{array}$	- 0.6566 .6568 .6569 .6569 .6564	- 0.6558 .6552 .6543 .6543 .6533	- 0.6508 .6494 .6478 .6478 .6440	- 0.6422 .6401 .6378 .6355 .6331	$\begin{array}{c} -0.6305\\ .6279\\ .6252\\ .6224\\ .6195\end{array}$	-0.6165
ETY	$\mathscr{I} G(\rho)$	17°	-0.6267 -6302 -6335 -6335 -6364 -6392	- 0.6417 .6439 .6459 .6457 .6477	- 0.6505 -6516 -6525 -6531 -6531	- 0.6538 - 6539 - 6538 - 6535 - 6535 - 6530	- 0.6523 .6515 .6505 .6494 .6481	- 0-6467 - 6452 - 6435 - 6416 - 6397	- 0-6376 -6354 -6331 -6338 -6308 -6283	- 0-6257 - 6230 - 6230 - 6202 - 6144	-0.6114
SOCI		16°	- 0.6267 -6300 -6330 -6330 -63358 -6384	- 0.6407 - 6427 - 6445 - 6461 - 6474	- 0.6486 -6495 -6502 -6507 -6509	- 0.6511 -6510 -6507 -6503 -6496	- 0.6489 - 6479 - 6468 - 6468 - 6442	- 0.6427 - 6410 - 6392 - 6353 - 6353	- 0.6331 -6309 -6285 -6285 -6235	- 0.6208 .6181 .6153 .6124 .6094	-0.6064
0F		15°	-0.6267 .6298 .6326 .6352 .6375	- 0-6396 -6415 -6431 -6431 -6445	-0.6466 .6473 .6479 .6482 .6483	-0.6483 .6480 .6476 .6471 .6471	-0-6454 -6443 -6431 -6431 -6418 -6403	- 0.6386 -6369 -6350 -6330 -6330	-0.6287 -6263 -6239 -6239 -6214 -6188	-0.6161 -6133 -6104 -6075 -6045	-0.6014
•		19°	+ 0.6267 -6148 -6030 -5913 -5796	+ 0.5680 .5564 .5449 .5335 .5335	+ 0-5109 -4997 -4886 -4776 -4776 -4667	+ 0.4560 -4453 -4453 -4347 -4347 -4243 -4140	+0-4038 -3937 -3837 -3837 -3837 -3642	+0.3546 .3451 .3451 .3358 .3358 .3266 .3176	+0-3087 -2999 -2913 -2913 -2828 -2745	+0-2662 -2582 -2502 -2424 -2348	+0.2272
ENCES		18 °	+ 0.6267 $\cdot 6148$ $\cdot 6029$ $\cdot 5911$ $\cdot 5794$	+ 0.5677 .5561 .5446 .5332 .5219	+ 0-5106 -4994 -4884 -4774 -4666	+ 0-4559 -4452 -4452 -4347 -4243 -4141	+ 0-4039 -3939 -3840 -3743 -3743 -3647	+0.3552 .3458 .3366 .3275 .3186	+0.3098 $\cdot 3011$ $\cdot 2925$ $\cdot 2842$ $\cdot 2759$	+0-2678 -2598 -2520 -2443 -2367	+0.2293
	$\mathscr{R}G(ho)$	17°	+ 0.6267 $\cdot 6147$ $\cdot 6028$ $\cdot 5910$ $\cdot 5792$	$\begin{array}{c} + \ 0.5675 \\ .5559 \\ .5444 \\ .5329 \\ .5216 \end{array}$	+0.5104 $\cdot4992$ $\cdot4882$ $\cdot4773$ $\cdot4665$	+0.4558 $\cdot4452$ $\cdot4348$ $\cdot4348$ $\cdot4244$ $\cdot4142$	+ 0-4042 -3942 -3844 -3747 -3652	+0.3558 .3465 .3374 .3284 .3196	+0.3108 $\cdot 3023$ $\cdot 2938$ $\cdot 2855$ $\cdot 2774$	+0.2694 -2615 -2538 -2462 -2388	+0.2314
SOCIETY	- 0	16 °	+0.6267 $\cdot 6146$ $\cdot 6027$ $\cdot 5908$ $\cdot 5790$	+0.5673 .5557 .5442 .5327 .5214	+0.5102 -4991 -4881 -4772 -4664	+ 0.4558 $\cdot 4452$ $\cdot 4349$ $\cdot 4246$ $\cdot 4145$	+ 0.4045 $\cdot 3946$ $\cdot 3848$ $\cdot 3752$ $\cdot 3658$	+ 0.3565 $\cdot 3473$ $\cdot 3382$ $\cdot 3293$ $\cdot 3206$	+ 0.3120 -3035 -2952 -2870 -2789	+0.2710 -2632 -2556 -2481 -2408	+0.2336
		p 15°	+ 0.6267 .6146 .6026 .5907 .5789	+0.5671 .5555 .5440 .5325 .5212	+ 0-5100 -4989 -4880 -4771 -4664	+ 0-4558 -4453 -4453 -4350 -4248 -4147	+0-4048 -3950 -3853 -3853 -3758 -3664	+0.3572 $\cdot 3481$ $\cdot 3391$ $\cdot 3303$ $\cdot 3217$	+0.3131 $\cdot 3048$ $\cdot 2965$ $\cdot 2884$ $\cdot 2805$	+0.2727 -2650 -2575 -2501 -2428	+0.2357
0F		$\left \rho\right $	0-00 01 03 04	0-05 -06 -07 -08 -09	0:10 11 12 13	0.15 .16 .17 .17 .19	0:20 22 24 23	0:25 :26 :27 :28 :29	0:30 31 32 33 34	0:35 36 37 38 38 39	0.40

					ON THE	COMPLEX	K VALUES	OF ρ		201	
YSICAL ENGINEERING IENCES		19 °	-0.6217 .6187 .6156 .6124 .6092		-0.5885 .5849 .5813 .5776 .5739	-0.5701 -5664 -5626 -5587 -5549	$\begin{array}{c} -0.5510\\ .5472\\ .5433\\ .5333\\ .5394\\ .5355\end{array}$	$\begin{array}{c} -0.5316\\ \cdot5276\\ \cdot5237\\ \cdot5198\\ \cdot5159\end{array}$	$\begin{array}{c} - \ 0.5120 \\ .5080 \\ .5041 \\ .5002 \\ .4963 \end{array}$	-0.4925 -4886 -4848 -4848 -4809 -4771	-0.4733
& EN BHYS		18 °	-0.6165 .6135 .6135 .6103 .6072 .6039	$\begin{array}{c} -0.6006\\ \cdot 5972\\ \cdot 5938\\ \cdot 5903\\ \cdot 5903\\ \cdot 5868\\ \cdot 5868\end{array}$	- 0-5833 -5797 -5760 -5724 -5687	$\begin{array}{c} -0.5649\\ \cdot5612\\ \cdot5574\\ \cdot5536\\ \cdot5498\\ \cdot5498\end{array}$	- 0-5460 -5421 -5421 -5383 -5306 -5306	$\begin{array}{c} -0.5267\\ \cdot5228\\ \cdot5189\\ \cdot5151\\ \cdot5112\end{array}$	- 0.5073 .5035 .4996 .4958 .4920	- 0:4881 -4843 -4805 -4805 -4730	-0.4693
CIETY	$\mathscr{I} G(\rho)$	17°	$\begin{array}{c} - \ 0.6114 \\ \cdot \ 0.83 \\ \cdot \ 0.6052 \\ \cdot \ 0.6020 \\ \cdot \ 0.5987 \\ \cdot \ 5987 \end{array}$	-0-5954 -5920 -5886 -5851 -5816	$\begin{array}{c} -0.5781\\ \cdot 5745\\ \cdot 5708\\ \cdot 5672\\ \cdot 5635\\ \cdot 5635\end{array}$	-0-5598 -5561 -5523 -5486 -5448	$\begin{array}{c} -0.5410\\ .5372\\ .5334\\ .5336\\ .5296\\ .5257\end{array}$	$\begin{array}{c} -0.5219\\ \cdot 5181\\ \cdot 5142\\ \cdot 5104\\ \cdot 5104\\ \cdot 5066\end{array}$	- 0.5028 .4990 .4952 .4914 .4876	-0-4839 -4801 -4764 -4727 -4727 -4690	-0.4653
rions SO		16°	-0.6064 -0.033 -6001 -5969 -5936	-0-5903 -5869 -5835 -5830 -5800 -5765	-0-5729 -5693 -5657 -5621 -5621	-0.5548 .5511 .5473 .5436 .5338	$\begin{array}{c} -0.5361\\ \cdot 5323\\ \cdot 5323\\ \cdot 5285\\ \cdot 5248\\ \cdot 5210\end{array}$	-0.5172 .5134 .5096 .5059 .5021	-0-4983 -4946 -4908 -4871 -4871	$\begin{array}{c} -0.4797\\ \cdot4760\\ \cdot4723\\ \cdot4723\\ \cdot4650\\ \cdot4650\end{array}$	-0.4614
		15°	-0.6014 -5983 -5951 -5919 -5886	-0-5852 -5818 -5784 -5749 -5714	-0-5679 -5643 -5607 -5571 -5535	-0.5498 .5461 .5424 .5327 .5350	-0.5313 .5275 .5238 .5238 .5200 .5163	-0-5126 -5088 -5051 -5013 -4976	$\begin{array}{c} -0.4939\\ -4902\\ \cdot4865\\ \cdot4828\\ \cdot4828\\ \cdot4792\end{array}$	$\begin{array}{c} -0.4755\\ \cdot4719\\ \cdot4719\\ \cdot4682\\ \cdot4646\\ \cdot4610\\ \cdot4610\end{array}$	-0.4575
		19°	+0.2272 -2199 -2126 -2055 -1985	+0.1917 $\cdot 1850$ $\cdot 1784$ $\cdot 1720$ $\cdot 1657$	+0.1595 $\cdot 1535$ $\cdot 1476$ $\cdot 1418$ $\cdot 1361$	+0.1306 $\cdot 1252$ $\cdot 1199$ $\cdot 1147$ $\cdot 1096$	+ 0.1047 - 0999 - 0952 - 0906 - 0861	+ 0.0817 -0774 -0733 -0692 -0652	+0.0614 0.0576 0.0539 0.0504 0.0469	+0.0435 0.0402 0.0370 0.0339 0.0309	+0.0279
PHYSICAL & ENGINEERING SCIENCES		18 °	+0.2293 $\cdot 2221$ $\cdot 2149$ $\cdot 2079$ $\cdot 2010$	+0-1943 -1877 -1812 -1812 -1749 -1687	+ 0-1626 -1567 -1567 -1509 -1452 -1396	+0.1342 $\cdot 1288$ $\cdot 1236$ $\cdot 1185$ $\cdot 1136$	+0.1087 -1087 -0993 -0948 -0904	+ 0.0861 -0819 -0819 -0738 -0738 -0699	+0-0661 -0624 -0588 -0553 -0519	+0-0486 -0453 -0453 -0422 -0391	+0.0332
YA	$\mathscr{R}G(ho)$	17°	+0.2314 -2243 -2172 -2103 -2036	+0.1969 $\cdot 1904$ $\cdot 1841$ $\cdot 1778$ $\cdot 1717$	+0.1658 $\cdot 1599$ $\cdot 1542$ $\cdot 1436$ $\cdot 1431$	+0.1377 $\cdot 1325$ $\cdot 1274$ $\cdot 1224$ $\cdot 1175$	+ 0.1127 $\cdot 1081$ $\cdot 1035$ $\cdot 0991$ $\cdot 0947$	+0.0905 -0863 -0823 -0784 -0745	+0.0708 -0672 -0636 -0602 -0568	+0.0535 0.503 0.472 0.442 0.412 0.412	+0.0384
SOCIETY	~0	16 °	+0.2336 -2265 -2196 -2128 -2128 -2061	+ 0.1996 $\cdot 1932$ $\cdot 1869$ $\cdot 1808$ $\cdot 1748$	$\begin{array}{c} + \ 0.1689 \\ \cdot 1631 \\ \cdot 1575 \\ \cdot 1575 \\ \cdot 1520 \\ \cdot 1466 \end{array}$	+0.1413 $\cdot 1361$ $\cdot 1311$ $\cdot 1262$ $\cdot 1214$	+ 0.1167 + 0.1167 - 0.1026 - 0.032 - 0.0990 - 0.0990 - 0.0900 - 0.0900 - 0.0900 - 0.0990 -	+0.0948 -0907 -0868 -0829 -0791	+0.0754 -0719 -0684 -0649 -0616	+0.0584 0.0552 0.522 0.492 0.463	+0.0434
TRANSACTIONS		15°	+0.2357 -2288 -2219 -2152 -2087	+0.2022 $\cdot 1959$ $\cdot 1897$ $\cdot 1837$ $\cdot 1778$	+0.1720 $\cdot 1663$ $\cdot 1608$ $\cdot 1553$ $\cdot 1500$	+0.1448 $\cdot 1398$ $\cdot 1348$ $\cdot 1348$ $\cdot 1300$ $\cdot 1252$	+0.1206 $\cdot 1161$ $\cdot 1117$ $\cdot 1074$ $\cdot 1032$	+0.0991 -0951 -0912 -0873 -0836	+0.0800 -0765 -0730 -0697	+0.0632 -0601 -0571 -0541 -0512	+0.0485
TRANSAC		$\frac{\operatorname{arg}\rho}{ \rho }$	040 41 43 44 44	0.45 46 47 48	050 53 53 53 53	0 5 5 5 7 5 7 5 7 6 5 7 6 5 7 7 7 7 7 7 7	0-60 61 64 64 64 64 64 64 64 64 64 64 64 64 64	0.65 66 68 69	0.70 .71 .73 .73	0.75 .76 .78 .78 .78	0.80

THE ROYAL A MATHEMATICAL PHILOSOPHICAL PHILOSOPHICAL

THE ROYAL A MATHEMATICAL TRANSACTIONS

			202	P. C.	CLEMMO	OW AND C	CARA M. I	MUNFORI)		
EERING		24°	$\begin{array}{c} - 0.6267\\ .6316\\ .6316\\ .6363\\ .6407\\ .6449\end{array}$		- 0.6642 .6666 .6687 .6705 .6722	- 0.6736 .6748 .6757 .6757 .6765	- 0.6774 - 6775 - 6775 - 6775 - 6772	$\begin{array}{c} -0.6762\\ .6754\\ .6744\\ .6733\\ .6733\\ .6720\end{array}$	- 0.6706 .6690 .6673 .6673 .6654	$\begin{array}{c} - \ 0.6612 \\ .6589 \\ .6565 \\ .6540 \\ .6514 \end{array}$	-0.6487
& ENGINEERING SCIENCES	ŗ	23°	- 0.6267 -6314 -6314 -6359 -6401 -6441	$\begin{array}{c} - 0.6477 \\ .6511 \\ .6543 \\ .6543 \\ .6572 \\ .6598 \end{array}$	- 0.6623 -6644 -6663 -6680 -6695	- 0.6707 - 6718 - 6726 - 6732 - 6735	- 0.6737 .6737 .6735 .6731 .6731	$\begin{array}{c} - \ 0.6719 \\ .6709 \\ .6699 \\ .6686 \\ .6672 \\ .6672 \end{array}$	- 0.6657 - 6640 - 6622 - 6602 - 6581	- 0.6559 - 6536 - 6511 - 6511 - 6459	-0.6431
SOCIETY 1	$\mathscr{I} G(\rho)$	22°	- 0.6267 .6312 .6355 .6395 .6432	$\begin{array}{c} - 0.6467 \\ \cdot 6499 \\ \cdot 6529 \\ \cdot 6556 \\ \cdot 6581 \end{array}$	- 0.6603 .6623 .6640 .6640 .6655	$\begin{array}{c} -0.6679\\ \cdot 6687\\ \cdot 6694\\ \cdot 6698\\ \cdot 6698\\ \cdot 6701\end{array}$	$\begin{array}{c} -0.6701\\ \cdot 6700\\ \cdot 6696\\ \cdot 6691\\ \cdot 6684\\ \cdot 6684\end{array}$	- 0.6676 .6665 .6654 .6640 .6625	$\begin{array}{c} - 0.6609\\ \cdot 6591\\ \cdot 6572\\ \cdot 6552\\ \cdot 6530\\ \cdot 6530\end{array}$	- 0.6507 .6483 .6458 .6458 .6405	-0.6376
		21°	$\begin{array}{c} - 0.6267 \\ \cdot 6310 \\ \cdot 6351 \\ \cdot 6389 \\ \cdot 6424 \end{array}$	- 0.6457 .6487 .6515 .6540 .6563	$\begin{array}{c} - 0.6583 \\ \cdot 6601 \\ \cdot 6617 \\ \cdot 6617 \\ \cdot 6630 \\ \cdot 6632 \end{array}$	- 0.6651 .6657 .6662 .6665 .6665	- 0.6665 .6662 .6657 .6651 .6651	$\begin{array}{c} - 0.6633 \\ \cdot 6622 \\ \cdot 6609 \\ \cdot 6594 \\ \cdot 6579 \end{array}$	$\begin{array}{c} - \ 0.6561 \\ \cdot \ 6543 \\ \cdot \ 6523 \\ \cdot \ 6522 \\ \cdot \ 6479 \end{array}$	- 0.6456 -6431 -6431 -6405 -6379 -6351	-0.6322
I KANSACI IUNS		20 °	- 0.6267 .6308 .6308 .6347 .6343 .6383		-0.6564 .6580 .6594 .6605 .6615	- 0-6622 -6628 -6631 -6632 -6632 -6632	- 0-6629 -6625 -6619 -6611 -6602	- 0.6591 .6579 .6565 .6565 .6549	$\begin{array}{c} - 0.6514 \\ 0.6514 \\ 0.6495 \\ 0.6474 \\ 0.6452 \\ 0.6429 \end{array}$	- 0-6405 -6380 -6380 -6354 -6326 -6326	-0.6269
-		24°	+0.6267 .6152 .6037 .5923 .5808	+0.5694 .5580 .5466 .5352 .5239	+0.5126 .5014 .4902 .4791 .4681	+0.4571 -4462 -4354 -4247 -4141	+0-4035 -3931 -3828 -3828 -3725 -3624	+0.3524 -3425 -3327 -3231 -3231 -3135	+0.3041 .2948 .2857 .2767 .2678	+ 0-2590 -2503 -2418 -2335 -2335	+0.2172
INGINEERING ENCES		2 3°	+0.6267 -6151 -6036 -5921 -5806	+0.5691 .5576 .5462 .5348 .5235	+0.5122 .5010 .4898 .477	+0.4568 -4460 -4352 -4352 -4245 -4140	+0-4035 -3931 -3829 -3829 -3727 -3627	+0.3527 .3429 .3333 .3237 .3237 .3143	+0-3050 -2958 -2867 -2867 -2867 -2890	+0-2604 -2518 -2435 -2435 -2352 -2271	+0.2191
	$\mathscr{R}G(ho)$	22°	+0.6267 -6150 -6034 -5919 -5803	+0.5688 .5573 .5458 .5344 .5231	+0.5118 .5006 .4895 .4784 .4674	+0-4565 -4457 -4350 -4350 -4244 -4139	+ 0-4035 -3932 -3830 -3830 -3830 -3630	+0-3531 -3434 -3338 -3338 -3338 -3244 -3150	+ 0-3058 -2967 -2878 -2878 -2790 -2703	+0-2618 -2534 -2451 -2451 -2370 -2290	+0.2211
SOCIETY	02	21 °	+0.6267 .6150 .6033 .5917 .5800	+0.5685 .5570 .5455 .5341 .5227	+0.5115 .5003 .4891 .4781 .4672	+0.4563 $\cdot4455$ $\cdot4359$ $\cdot4349$ $\cdot4243$ $\cdot4139$	+ 0-4035 - 3933 - 3832 - 3832 - 3732 - 3633	+ 0:3536 :3439 :3344 :3251 :3158	+ 0.3067 -2978 -2889 -2802 -2716	+0.2632 -2549 -2468 -2468 -2388 -2309	+0.2231
		o 20°	+0.6267 $\cdot 6149$ $\cdot 6032$ $\cdot 5915$ $\cdot 5798$	+0.5682 .5567 .5452 .5338 .5224	+ 0.5111 $\cdot 5000$ $\cdot 4888$ $\cdot 4778$ $\cdot 4669$	+ 0.4561 $\cdot 4454$ $\cdot 4348$ $\cdot 4348$ $\cdot 4243$ $\cdot 4139$	+ 0.4036 .3935 .3834 .3735 .3735	+0.3540 $\cdot3445$ $\cdot3351$ $\cdot3258$ $\cdot3167$	+ 0.3077 -2988 -2901 -2815 -2730	+ 0.2647 -2565 -2485 -2406 -2328	+0.2252
KANSACIIUNS OF	Ĩ	$\left \rho\right $	0.0 0.0 0,0 0,0 0,0 0,0 0,0 0,0 0,0 0,0	0.05 06 08 09 09	0:10 11 12 13 14	0.15 .16 .17 .18 .19	0-20 21 23 23 24	0:25 :26 :28 :29	0:30 :31 :33 :33 :34	0:35 :36 :37 :38 :39	0.40

TRANSACTIONS CONTINUE & MATHEMATICAL BHILDSOPHICAL BHYLDSOPHICAL

TRANSACTIONS COLLETV

					ON THE	COMPLEX	VALUES	OF ρ		203	
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		24°	-0.6487 .6458 .6429 .63399 .6367	$\begin{array}{c} - 0.6335 \\ \cdot 6302 \\ \cdot 6302 \\ \cdot 6269 \\ \cdot 6234 \\ \cdot 6199 \end{array}$	$\begin{array}{c} - 0.6163\\ \cdot 6127\\ \cdot 6090\\ \cdot 6053\\ \cdot 6015\\ \cdot 6015\end{array}$	$\begin{array}{c} -0.5976\\ \cdot5937\\ \cdot5898\\ \cdot5858\\ \cdot5818\\ \cdot5818\end{array}$	$\begin{array}{c} -0.5778 \\ \cdot 5737 \\ \cdot 5696 \\ \cdot 5655 \\ \cdot 5613 \end{array}$	- 0.5572 .5530 .5488 .5446 .5404	$\begin{array}{c} - \ 0.5362 \\ .5320 \\ .5278 \\ .5278 \\ .5236 \\ .5194 \end{array}$	$\begin{array}{c} -0.5152\\ .5110\\ .5069\\ .5069\\ .5027\\ .4985\end{array}$	-0.4944
Y		23 °	-0.6431 .6402 .6373 .6373 .6310	-0-6278 -6245 -6211 -6177 -6142	- 0-6106 -6070 -5033 -5995 -5957	$\begin{array}{c} - 0.5919\\ \cdot 5880\\ \cdot 5841\\ \cdot 5802\\ \cdot 5762\\ \cdot 5762\end{array}$	-0.5722 .5682 .5641 .5601 .5560	-0-5519 -5478 -5436 -5395 -5354	-0-5312 -5271 -5229 -5188 -5147	$\begin{array}{c} -0.5105\\ \cdot 5064\\ \cdot 5023\\ \cdot 4982\\ \cdot 4941\end{array}$	
THE ROYAL SOCIETY	$\mathscr{I} G(\rho)$	33°	-0.6376 -6347 -6317 -6317 -6286 -6254	- 0.6222 .6189 .6155 .6120 .6085	-0.6049 -6013 -5976 -5939 -5901	- 0.5863 .5825 .5786 .5747 .5707	- 0.5668 .5628 .5588 .5547 .5547	- 0.5466 .5426 .5385 .5385 .5344 .5304	$\begin{array}{c} -0.5263\\ \cdot 5222\\ \cdot 5181\\ \cdot 5140\\ \cdot 5100\end{array}$	$\begin{array}{c} -0.5059\\ .5018\\ .4978\\ .4938\\ .4898\\ .4898\end{array}$	-0.4858
		21 °	-0.6322 .6293 .6293 .6263 .6231 .6199	-0.6167 -6133 -6099 -6095 -6030	-0.5994 .5958 .5921 .5884 .5846	- 0.5808 .5770 .5732 .5693 .5654	-0.5614 .5575 .5535 .5495 .5455	-0-5415 -5375 -5335 -5295 -5254	-0.5214 .5174 .5134 .5094 .5053	-0.5013 -4974 -4934 -4894 -4855	-0.4815
PHILOSOPHICAL TRANSACTIONS		20°	- 0.6269 -6239 -6239 -6177 -6145	$\begin{array}{c} -0.6112\\ \cdot 6079\\ \cdot 6045\\ \cdot 6010\\ \cdot 5975\end{array}$	$\begin{array}{c} -0.5939\\ \cdot5903\\ \cdot5866\\ \cdot5829\\ \cdot5792\\ \cdot5792\end{array}$	-0.5754 .5716 .5678 .5640 .5641	-0-5562 -5523 -5483 -5444 -5405	- 0-5365 -5325 -5326 -5286 -5246 -5206	-0-5166 -5127 -5087 -5087 -5008	$\begin{array}{c} -0.4969\\ \cdot4929\\ \cdot4890\\ \cdot4851\\ \cdot4812\\ \cdot4812\end{array}$	
		24°	+0.2172 -2092 -2014 -1937 -1862	+0.1788 $\cdot 1715$ $\cdot 1644$ $\cdot 1574$ $\cdot 1505$	+0.1438 $\cdot 1372$ $\cdot 1308$ $\cdot 1245$ $\cdot 1183$	+0.1122 $\cdot 1063$ $\cdot 1005$ $\cdot 0949$ $\cdot 0894$	+0-0840 -0787 -0735 -0685 -0636	+ 0-0588 -0541 -0496 -0451 -0408	+0.0366 -0325 -0325 -0285 -0246 -0208	+0.0172 0.0136 0.0101 0.0067 0.0034	+0.0003
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		23°	+0.2191 $\cdot 2113$ $\cdot 2036$ $\cdot 1960$ $\cdot 1886$	+0.1813 -1742 -1672 -1603 -1536	+0.1470 $\cdot 1405$ $\cdot 1342$ $\cdot 1280$ $\cdot 1219$	+ 0.1159 - 1101 - 1045 - 0989 - 0935	+ 0.0882 -0830 -0779 -0730 -0730	+0-0635 -0589 -0544 -0544 -0501	+0-0417 -0377 -0337 -0337 -0299 -0262	+0-0226 -0191 -0157 -0124 -0091	+0.0060
	$\mathscr{R} G(ho)$	22 °	+0.2211 $\cdot 2134$ $\cdot 2058$ $\cdot 1984$ $\cdot 1911$	+0.1839 $\cdot 1769$ $\cdot 1700$ $\cdot 1632$ $\cdot 1566$	$\begin{array}{c} + 0.1501 \\ - 1437 \\ - 1375 \\ - 1314 \\ - 1314 \\ - 1255 \end{array}$	+0.1196 $\cdot 1139$ $\cdot 1083$ $\cdot 1029$ $\cdot 0976$	+0.0924 -0873 -0823 -0775 -0727	+ 0.0681 -0636 -0592 -0550 -0508	+0.0467 -0428 -0389 -0352 -0315	+0.0280 -0245 -0211 -0179 -0147	+0.0116
THE ROYAL Society		21°	+0.2231 $\cdot 2155$ $\cdot 2081$ $\cdot 2007$ $\cdot 1935$	+0.1865 -1796 -1728 -1661 -1661	$\begin{array}{c} + 0.1532 \\ - 1470 \\ - 1409 \\ - 1349 \\ - 1349 \\ - 1290 \end{array}$	+0.1233 $\cdot1177$ $\cdot1122$ $\cdot1069$ $\cdot1016$	+0.0965 -0915 -0866 -0819 -0772	+0.0727 $\cdot0683$ $\cdot0640$ $\cdot0598$ $\cdot0557$	+0.0517 0.478 0.440 0.403 0.367	+0.0332 0.298 0.265 0.233 0.202	+0.0171
TRANSACTIONS		. ρ 20 °	+ 0.2252 + 0.2252 - 0.2177 - 0.2103 - 0.2031 - 0.2031 - 0.1960 -	$\begin{array}{c} + \ 0.1891 \\ - \ 1823 \\ \cdot 1756 \\ \cdot 1756 \\ \cdot 1691 \\ \cdot 1627 \end{array}$	+0.1564 $\cdot 1502$ $\cdot 1442$ $\cdot 1383$ $\cdot 1326$	+0.1269 -1214 -1161 -1108 -1056	+0.1006 -0.957 -0.909 -0.862 -0.817	+0.0772 -0729 -0686 -0645 -0605	+ 0.0566 -0527 -0490 -0454 -0419	+0.0384 $\cdot 0.351$ $\cdot 0.318$ $\cdot 0.287$ $\cdot 0.256$	+0.0226
PHILOS TRANS		$\frac{\operatorname{arg}\rho}{ \rho }$	0-40 -41 -42 -43 -43	0:45 :46 :47 :48 :48	0:50 5:1 5:3 5:4 5:4	0:55 56 57 58 59	0 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.65 66 68 69	0·70 ·71 ·72 ·73 ·74	0.75 .76 .77 .78 .79	0.80

			204	P. C.	CLEMMO	OW AND (CARA M.	MUNFOR	D		
S		29°		- 0.6537 .6583 .6628 .6626 .6667	- 0.6740 .6773 .6804 .6832 .6832	- 0.6880 .6901 .6919 .6935 .6935	- 0.6960 - 6969 - 6976 - 6980 - 6983	0.6984 		-0.6887 .6868 .6868 .6848 .6826 .6802	-0.6778
SCIENCE		28°	- 0.6267 - 0.324 - 6379 - 6431 - 6480	- 0.6527 .6571 .6612 .6612 .6651	- 0.6721 .6752 .6780 .6806 .6830	- 0.6851 .6870 .6886 .6900 .6912	$\begin{array}{c} - 0.6922\\ \cdot 6929\\ \cdot 6935\\ \cdot 6938\\ \cdot 6938\\ \cdot 6939\end{array}$	- 0-6938 -6936 -6931 -6931 -6916	- 0.6906 - 6894 - 6881 - 6885 - 6849	- 0.6830 .6811 .6789 .6743 .6743	-0.6718
ELY	$\mathscr{I}G(\rho)$	27°	- 0.6267 .6322 .6375 .6425 .6472	- 0.6517 .6559 .6598 .6635 .6635	- 0.6701 .6730 .6757 .6757 .6803	$\begin{array}{c} - 0.6822\\ \cdot 6839\\ \cdot 6834\\ \cdot 6866\\ \cdot 6866\\ \cdot 6877\end{array}$	- 0.6885 .6891 .6894 .6896 .6896	- 0.6894 .6890 .6884 .6876 .6876	$\begin{array}{c} - 0.6855 \\ \cdot 6842 \\ \cdot 6828 \\ \cdot 6828 \\ \cdot 6812 \\ \cdot 6794 \end{array}$	$\begin{array}{c} - 0.6775 \\ \cdot 6754 \\ \cdot 6732 \\ \cdot 6732 \\ \cdot 6709 \\ \cdot 6684 \end{array}$	-0.6659
SOCI		26°	$\begin{array}{c} -0.6267\\ \cdot 6320\\ \cdot 6371\\ \cdot 6419\\ \cdot 6464\\ \cdot 6464\end{array}$	- 0.6507 .6547 .6585 .6585 .6619	- 0.6681 .6709 .6733 .6736 .6776	$\begin{array}{c} - \ 0.6793 \\ \cdot \ 6809 \\ \cdot \ 6822 \\ \cdot \ 6832 \\ \cdot \ 6841 \\ \cdot \ 6841 \end{array}$	- 0.6848 .6852 .6854 .6855 .6855	- 0.6849 .6844 .6837 .6828 .6817	$\begin{array}{c} - \ 0.6805 \\ \cdot \ 6791 \\ \cdot \ 6775 \\ \cdot \ 6758 \\ \cdot \ 6740 \end{array}$	- 0.6720 .6698 .6676 .6652 .6652	-0.6600
OF		25°	0.6267 	-0.6497 .6535 .6571 .6604 .6634	$\begin{array}{c} - \ 0.6662 \\ . 6687 \\ . 66710 \\ . 6731 \\ . 6749 \\ . 6749 \end{array}$	- 0.6765 .6778 .6778 .6789 .6789	- 0.6811 - 6813 - 6813 - 6814 - 6813 - 6810	- 0.6805 .6799 .6790 .6780 .6780	- 0.6755 .6740 .6724 .6724 .6706	- 0.6666 -6644 -6620 -6520 -6570	-0.6543
•		29°	+0-6267 -6157 -6046 -5935 -5824	+ 0.5712 -5600 -5488 -5376 -5264	+ 0.5152 .5040 .4928 .4816 .4705	+ 0.4594 -4483 -4483 -4373 -4373 -4264 -4155	+ 0.4046 .3939 .3832 .3726 .3620	+0.3516 .3412 .3310 .3208 .3108	+0.3008 -2910 -2813 -2717 -2622	+ 0.2528 -2436 -2344 -2344 -2255 -2166	+0.2079
ENCES		28°	+0.6267 .6156 .6044 .5933 .5821	+0.5708 .5596 .5483 .5371 .5371	+0.5146 .5034 .4922 .4810 .4699	+0.4588 -4478 -4368 -4259 -4151	+0-4043 -3936 -3830 -3830 -3724 -3620	+0.3516 .3414 .3312 .3312 .3312 .3312 .3112	+0.3014 -2917 -2820 -2820 -2726 -2632	+0.2539 -2448 -2358 -2358 -2270 -2182	+0.2096
	$\mathscr{R}G(ho)$	27 °	+0.6267 .6155 .6042 .5930 .5817	+0-5704 -5591 -5479 -5366 -5253	+0.5141 .5028 .4916 .4805 .4694	+0-4583 -4473 -4364 -4265 -4147	+0-4040 -3934 -3828 -3828 -3724 -3620	+0.3517 .3416 .3315 .3216 .3216 .3117	+ 0-3020 -2924 -2829 -2735 -2643	+0-2551 -2461 -2373 -2373 -2285 -2199	+0.2115
SUCLETY	03	26°	+0.6267 .6154 .6041 .5927 .5814	+0.5701 .5587 .5474 .5361 .5248	+0.5135 .5023 .4911 .4800 .4689	+ 0.4579 -4469 -4360 -4252 -4145	+0.4038 -3932 -3828 -3828 -3724 -3621	+0.3519 .3418 .3319 .320 .3123	+ 0.3026 -2931 -2838 -2838 -2838 -2745 -2654	+0.2564 $\cdot2475$ $\cdot2388$ $\cdot2301$ $\cdot2217$	+0.2133
SC		o 25°	+0.6267 $\cdot6153$ $\cdot6039$ $\cdot5925$ $\cdot5811$	+0.5697 .5583 .5470 .5356 .5243	+0.5131 .5018 .4907 .4795 .4685	+ 0.4575 $\cdot 4466$ $\cdot 4357$ $\cdot 4249$ $\cdot 4142$	+0.4037 $\cdot 3931$ $\cdot 3827$ $\cdot 3724$ $\cdot 3622$	+0.3521 $\cdot3421$ $\cdot3323$ $\cdot3225$ $\cdot3129$	+0.3034 -2940 -2847 -2756 -2665	+0.2577 -2489 -2403 -2318 -234	+0.2152
- JO		$\frac{\arg\rho}{ \rho }$	0.00 0.00 0.00 0.00	0.05 06 08 09 09	0.10 .11 .12 .13 .13	0.15 ·16 ·17 ·18 ·18	0:20 21 22 23 24	0:25 26 28 28 29	0:30 :31 :32 :33 :34	0:35 :36 :37 :38 :39	0.40

TRANSACTIONS COCTETY & MATHEMATICAL

TRANSACTIONS COCTETY & MATHEMATICAL

lL, VG		29 °	$\begin{array}{c} - 0.6778 \\ .6752 \\ .6725 \\ .6696 \\ .6667 \\ .6667 \end{array}$	-0.6636 .6604 .6571 .6537 .6503	$\begin{array}{c} -0.6467\\ \cdot 6431\\ \cdot 6431\\ \cdot 6393\\ \cdot 6325\\ \cdot 6317\\ \cdot 6317\end{array}$	$\begin{array}{c} -0.6277\\ \cdot 6237\\ \cdot 6196\\ \cdot 6115\\ \cdot 6113\end{array}$	$\begin{array}{c} -0.6071\\ \cdot 6028\\ \cdot 5985\\ \cdot 5942\\ \cdot 5898\end{array}$	$\begin{array}{c} -0.5854\\ \cdot5809\\ \cdot5764\\ \cdot5720\\ \cdot5674\end{array}$	$\begin{array}{c} - 0.5629\\ \cdot 5584\\ \cdot 5538\\ \cdot 5493\\ \cdot 5447\\ \cdot 5447\end{array}$	$\begin{array}{c} - 0.5401 \\ \cdot 5355 \\ \cdot 5310 \\ \cdot 5264 \\ \cdot 5218 \end{array}$	-0.5173
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		38 °	$\begin{array}{c} -0.6718\\ \cdot 6691\\ \cdot 6664\\ \cdot 6664\\ \cdot 6635\\ \cdot 6605\end{array}$	- 0.6574 .6542 .6509 .6509 .6440	$\begin{array}{c} - 0.6404\\ \cdot 6368\\ \cdot 6330\\ \cdot 6292\\ \cdot 6254\\ \cdot 6254\end{array}$	$\begin{array}{c} -0.6215\\ \cdot 6175\\ \cdot 6134\\ \cdot 6033\\ \cdot 6052\end{array}$	$\begin{array}{c} -0.6010\\ \cdot 5968\\ \cdot 5925\\ \cdot 5882\\ \cdot 5839\end{array}$	-0-5795 -5751 -5707 -5663 -5618	-0.5574 .5529 .5439 .5439 .5394	$\begin{array}{c} -0.5349\\ \cdot5304\\ \cdot5304\\ \cdot5260\\ \cdot5215\\ \cdot5170\end{array}$	-0.5125
TY ALA	$\mathscr{I} G(\rho)$	27 °	$\begin{array}{c} - \ 0.6659 \\ \cdot \ 6632 \\ \cdot \ 6603 \\ \cdot \ 6574 \\ \cdot \ 6574 \\ \cdot \ 6574 \end{array}$	$\begin{array}{c} - 0.6513\\ \cdot 6480\\ \cdot 6447\\ \cdot 6413\\ \cdot 6378\end{array}$	$\begin{array}{c} - 0.6342 \\ \cdot 6306 \\ \cdot 6306 \\ \cdot 6269 \\ \cdot 6231 \\ \cdot 6192 \end{array}$	$\begin{array}{c} - \ 0.6153 \\ \cdot \ 6114 \\ \cdot \ 6073 \\ \cdot \ 6033 \\ \cdot \ 5992 \end{array}$	-0.5950 .5908 .5866 .5823 .5781	- 0.5737 .5694 .5651 .5667 .5607	$\begin{array}{c} - 0.5519\\ .5475\\ .5431\\ .5387\\ .5343\\ .5343\end{array}$	- 0.5299 .5255 .5210 .5166 .5123	-0.5079
THE RC SOCIE		26°	$\begin{array}{c} - 0.6600\\ .6573\\ .6573\\ .6544\\ .6515\\ .6484\\ .6484\end{array}$	$\begin{array}{c} - \ 0.6452 \\ \cdot \ 6420 \\ \cdot \ 6387 \\ \cdot \ 6387 \\ \cdot \ 6317 \end{array}$	$\begin{array}{c} - 0.6282\\ \cdot 6245\\ \cdot 6208\\ \cdot 6170\\ \cdot 6132\end{array}$	$\begin{array}{c} - 0.6093 \\ \cdot 6054 \\ \cdot 6014 \\ \cdot 5973 \\ \cdot 5933 \end{array}$	$\begin{array}{c} -0.5891\\ \cdot5850\\ \cdot5850\\ \cdot5706\\ \cdot5724\\ \cdot5724\end{array}$	- 0.5681 .5638 .5536 .5552 .5509	- 0.5466 .5423 .5379 .5336 .5336	$\begin{array}{c} - 0.5249\\ \cdot 5206\\ \cdot 5162\\ \cdot 5119\\ \cdot 5119\\ \cdot 5076\end{array}$	-0.5033
PHILOSOPHICAL TRANSACTIONS		25 °	- 0.6543 .6515 .6515 .6456 .6425	$\begin{array}{c} -0.6393\\ \cdot 6361\\ \cdot 6327\\ \cdot 6327\\ \cdot 6293\\ \cdot 6258\end{array}$	$\begin{array}{c} - 0.6222\\ \cdot 6186\\ \cdot 6149\\ \cdot 6111\\ \cdot 6073\end{array}$	- 0.6034 .5995 .5955 .5915 .5875	- 0.5834 .5793 • .5751 .5710 .5668	- 0-5626 - 5584 - 5541 - 5499 - 5456	- 0-5414 -5371 -5328 -5286 -5243	$\begin{array}{c} - 0.5200\\ \cdot 5158\\ \cdot 5115\\ \cdot 5073\\ \cdot 5073\\ \cdot 5030\end{array}$	-0.4988
TRAN		29°	+0.2079 $\cdot 1993$ $\cdot 1908$ $\cdot 1825$ $\cdot 1743$	+0.1662 $\cdot 1583$ $\cdot 1505$ $\cdot 1429$ $\cdot 1354$	+0.1281 $\cdot 1208$ $\cdot 1138$ $\cdot 1068$ $\cdot 1000$	+0.0934 -0869 -0805 -0743 -0682	+0.0622 -0564 -0507 -0451 -0397	$\begin{array}{c} + 0.0344 \\ \cdot 0.293 \\ \cdot 0.242 \\ \cdot 0193 \\ \cdot 0146 \end{array}$	+0.0099 -0054 +0.0010 -0.0033 -0075	$\begin{array}{c} - \ 0.0115 \\ \cdot \ 0.154 \\ \cdot \ 0.192 \\ \cdot \ 0.230 \\ \cdot \ 0.265 \end{array}$	-0.0300
IATHEMATICAL, HYSICAL E ENGINEERING CIENCES		28°	+0.2096 $\cdot 2012$ $\cdot 1928$ $\cdot 1847$ $\cdot 1766$	+0.1687 $\cdot 1609$ $\cdot 1533$ $\cdot 1458$ $\cdot 1384$	+0.1312 $\cdot 1241$ $\cdot 1172$ $\cdot 1104$ $\cdot 1037$	+0.0972 0.0908 0.0846 0.785 0.725	+ 0.0666 .0609 .0554 .0499 .0446	+ 0-0394 -0394 -0344 -0295 -0246 -0200	+0.0154 0110 -0067 +0.0025 -0.0016	$\begin{array}{c} - \ 0.0056 \\ - \ 0.0094 \\ - \ 0.132 \\ - \ 0.168 \\ - \ 0.203 \end{array}$	-0.0237
& ENGIN SCIENCE	$\mathscr{R}G(ho)$	27°	+ 0.2115 -2031 -1949 -1869 -1790	+0.1712 $\cdot 1635$ $\cdot 1560$ $\cdot 1487$ $\cdot 1414$	+ 0.1344 $\cdot 1274$ $\cdot 1206$ $\cdot 1139$ $\cdot 1074$	+ 0.1010 -0947 -0886 -0826 -0768	+ 0-0710 -0654 -0600 -0546 -0494	+ 0-0444 -0394 -0346 -0299 -0253	+0.0208 -0165 -0123 -0082 -0042	+0.0035 -0.0035 .0072 .0108 .0142	-0.0176
ROYAL IETY	0	26°	+0.2133 -2051 -1971 -1891 -1813	+0-1737 -1662 -1662 -1588 -1516 -1445	+0.1375 $\cdot 1307$ $\cdot 1240$ $\cdot 1174$ $\cdot 1110$	+0-1048 -0986 -0926 -0867 -0810	+ 0-0754 -0699 -0645 -0593 -0542	+0-0492 -0444 -0396 -0350 -0305	+0.0262 -0219 -0178 -0137 -0098	+0.0060 +0.0023 -0.0013 .0048 .0082	-0.0115
NNS THE R		ρ 25 °	+0.2152 -2072 -1992 -1914 -1837	+0.1762 $\cdot 1688$ $\cdot 1616$ $\cdot 1545$ $\cdot 1475$	+0.1407 $\cdot 1340$ $\cdot 1274$ $\cdot 1210$ $\cdot 1147$	+0.1085 $\cdot 1025$ $\cdot 0966$ $\cdot 0908$ $\cdot 0852$	+0.0797 0.743 0.691 0.639 0.589	+ 0.0540 -0493 -0446 -0401 -0357	+0.0314 -0.272 -0.232 -0.192 -0.154	$\begin{array}{c} + \ 0.0116 \\ - \ 0.080 \\ - \ 0.044 \\ + \ 0.0010 \\ - \ 0.023 \end{array}$	-0.0056
PHILOSOPHICAL TRANSACTIONS		$\frac{\operatorname{arg}\rho}{ \rho }$	0.40 41 42 43	0.45 46 47 47 48	0:50 51 53 54 54	0:55 56 57 53 59 59	0.60 61 63 64	0.65 66 63 69	0-70 -71 -72 -73 -73	0.75 77 77: 77: 79: 79:	0.80

Vol. 245. A.

25

ON THE COMPLEX VALUES OF ρ

PHILOSOPHICAL THF ROVAT A MATHEMATICAL

PHILOSOPHICAL THF ROYAL A MATHEMATICAL

			206	P. C.	CLEMMO	OW AND (CARA M.	MUNFORI)		
ATICAL, L EERING S		34°	$\begin{array}{c} - \ 0.6267 \\ . 6335 \\ . 6402 \\ . 6465 \\ . 6526 \end{array}$	$\begin{array}{c} -0.6585\\ -6641\\ -6694\\ -6744\\ -6742\\ -6792\end{array}$	$\begin{array}{c} - \ 0.6838\\ .6880\\ .6921\\ .6921\\ .6958\\ .6993\end{array}$	$\begin{array}{c} - 0.7026\\ \cdot 7026\\ \cdot 7056\\ \cdot 7108\\ \cdot 7130\\ \cdot 7130\end{array}$	$\begin{array}{c} -0.7151\\ .7168\\ .7183\\ .7183\\ .7196\\ .7207\end{array}$	$\begin{array}{c} - \ 0.7215 \\ .7221 \\ .7225 \\ .7225 \\ .7226 \\ .7226 \end{array}$	$\begin{array}{c} -0.7224\\ \cdot 7219\\ \cdot 7213\\ \cdot 7204\\ \cdot 7193\end{array}$	$\begin{array}{c} -0.7181\\ \cdot 7167\\ \cdot 71167\\ \cdot 71151\\ \cdot 71133\\ \cdot 71113\end{array}$	-0.7092
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		33 °	-0.6267 -6334 -6338 -6398 -6460 -6519	$\begin{array}{c} - 0.6575 \\ - 6629 \\ - 6620 \\ - 6680 \\ - 6775 \\ - 6775 \end{array}$	$\begin{array}{c} - \ 0.6818 \\ .6859 \\ .6897 \\ .6893 \\ .6933 \\ .6966 \end{array}$	- 0.6996 -7024 -7050 -7073 -7073	-0.7112 .7128 .7141 .7163 .7162	- 0.7168 .7173 .7175 .7175 .7175	$\begin{array}{c} -0.7169\\ \cdot 7163\\ \cdot 7156\\ \cdot 7156\\ \cdot 7134\\ \cdot 7134\end{array}$	$\begin{array}{c} -0.7121\\ \cdot 7105\\ \cdot 7088\\ \cdot 7070\\ \cdot 7049\end{array}$	-0.7027
THE ROYAL SOCIETY	$\mathscr{I} G(\rho)$	32°	$\begin{array}{c} -0.6267\\ .6332\\ .6332\\ .6394\\ .6454\\ .6511\end{array}$	- 0.6566 - 0.6566 - 0.6618 - 0.613 - 0.757 - 6757	-0.6799 -0.8338 -6874 -6907 -6939	-0.6967 -6993 -7017 -7038 -7057	-0.7074 $\cdot 7088$ $\cdot 7100$ $\cdot 71109$ $\cdot 7116$	- 0.7121 .7124 .7125 .7124 .7124	-0.7116 .7108 .7099 .7075	- 0.7061 .7045 .7027 .7007 .6986	-0.6963
		31 °	$\begin{array}{c} -0.6267\\ .6330\\ .6330\\ .6390\\ .6448\\ .6503\end{array}$	- 0.6556 - 6606 - 6653 - 6698 - 6740	-0.6779 -6816 -6850 -6882 -6882 -6911	- 0.6938 - 6962 - 6984 - 7004 - 7021	- 0.7035 .7048 .7058 .7066 .7072	- 0.7075 -7076 -7076 -7073 -7073	-0.7062 .7054 .7044 .7032 .7032	-0.7002 .6985 .6966 .6946 .6924	-0.6901
PHILOSOPHICAL TRANSACTIONS		30°	-0.6267 -6328 -6328 -6387 -6442 -6496	-0.6546 .6594 .6640 .6682 .6722	-0.6760 .6795 .6827 .6857 .6884	-0.6909 -6931 -6951 -6969 -6984	-0.6997 $\cdot 7008$ $\cdot 7017$ $\cdot 7023$ $\cdot 7027$	-0.7029 .7029 .7027 .7023 .7017	-0.7010 .7000 .6989 .6975 .6975	-0-6944 -6926 -6906 -6885 -6863	-0.6839
9 T		34°	+0.6267 .6162 .6057 .5950 .5843	+ 0.5735 .5626 .5517 .5517 .5297	+0.5186 .5075 .4963 .4852 .4740	+ 0.4628 .4517 .4417 .4405 .4294 .4182	+ 0.4072 .3961 .3851 .3741 .3632	+0.3523 $\cdot3415$ $\cdot3308$ $\cdot3208$ $\cdot3201$ $\cdot3095$	+0.2990 -2886 -2783 -2783 -2681 -2580	+0.2480 -2381 -2383 -2283 -2283 -2186 -2090	+0.1996
THEMATICAL, (SICAL NGINEERING ENCES		33 °	+0.6267 -6161 -6054 -5947 -5839	+0.5730 .5621 .5511 .5400 .5290	+0-5178 -5067 -4955 -4844 -4732	+0-4621 -4509 -4398 -4398 -4286 -4176	+0-4065 -3955 -3846 -3737 -3737 -3628	+0.3520 .3413 .3307 .3201 .3097	+ 0-2993 -2890 -2788 -2687 -2587	+0-2488 -2390 -2294 -2108 -2104	+0.2011
	$\mathscr{R} G(ho)$	32°	+0.6267 -6160 -6052 -5944 -5835	+0.5725 .5615 .5505 .5394 .5283	+0.5171 .5060 .4948 .4836 .4725	+0.4613 -4502 -4391 -4391 -4280 -4170	+0-4060 -3950 -3841 -3733 -3733 -3625	+0-3518 -3412 -3307 -3202 -3202 -3098	+0.2996 -2894 -2793 -2693 -2595	+0-2497 -2401 -2306 -2212 -2113	+0.2028
THE ROYAL SOCIETY		31 °	+0.6267 -6159 -6050 -5941 -5831	+0.5721 .5610 .5499 .5388 .5276	+0-5164 -5053 -4941 -4829 -4718	+0-4606 -4495 -4384 -4274 -4164	+0-4055 -3946 -3837 -3837 -3837 -3833 -3623	+0-3517 -3411 -3307 -3307 -3203 -3101	+0-2999 -2898 -2799 -2700	+0-2507 -2412 -2318 -2318 -2325 -2134	+0.2044
		р 30 °	+0.6267 -6158 -6048 -5938 -5828	+0.5717 .5605 .5494 .5382 .5382	+0.5158 .5046 .4934 .4822 .4711	+0-4600 -4489 -4378 -4378 -4268 -4159	+0-4050 -3942 -3834 -3727 -3621	+0.3516 .3412 .3308 .3206 .3206 .3104	+ 0.3003 -2904 -2806 -2708 -2612	+ 0-2517 -2423 -2331 -2331 -2240 -2150	+0.2061
PHILOSOPHICAL TRANSACTIONS	:	$ \rho $	0-0 -01 -03 -05 -05 -00 -00 -00 -00 -00 -00 -00 -00	0-05 -06 -08 -09	0-10 -11 -13 -13 -14 -14 -10 -10 -10 -10 -10 -10 -10 -10 -10 -10	0.15 .16 .17 .18 .18	0:20 :21 :23 :23	0:25 :26 :28 :29	0:30 31 32 33 32	0.35 .36 .37 .38 .38	0.40

rical, :RING		34°	-0.7092 .7070 .7045 .7019 .6992	$\begin{array}{c} -0.6964\\ \cdot 6934\\ \cdot 6932\\ \cdot 6902\\ \cdot 6870\\ \cdot 6836\end{array}$	$\begin{array}{c} -0.6801\\ .6765\\ .6727\\ .6689\\ .6650\\ .6650\end{array}$	$\begin{array}{c} - 0.6610\\ \cdot 6569\\ \cdot 6527\\ \cdot 6484\\ \cdot 6484\\ \cdot 6441\end{array}$	-0.6397 .6352 .6306 .6260 .6214	-0.6167 -6119 -6071 -6023 -5974	- 0.5925 .5876 .5826 .5776 .5727	- 0.5676 .5626 .5576 .5526 .5526	-0.5425
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		33 °	-0.7027 $\cdot 7004$ $\cdot 6979$ $\cdot 6923$ $\cdot 6925$	- 0.6896 .6865 .6833 .6833 .6801 .6766	$\begin{array}{c} - 0.6731 \\ - 6695 \\ - 6658 \\ - 6620 \\ - 6580 \\ - 6580 \end{array}$	- 0.6540 .6500 .6458 .6415 .6415 .6372	$\begin{array}{c} - \ 0.6329 \\ \cdot \ 0.284 \\ \cdot \ 0.239 \\ \cdot \ 0.148 \\ \cdot \ 0.148 \end{array}$	$\begin{array}{c} - \ 0.6101 \\ \cdot \ 0.6054 \\ \cdot \ 0.007 \\ \cdot \ 5959 \\ \cdot \ 5911 \end{array}$	- 0-5863 - 5815 - 5766 - 5717 - 5717 - 5668	$\begin{array}{c} - \ 0.5619 \\ \cdot 5570 \\ \cdot 5520 \\ \cdot 5471 \\ \cdot 5422 \end{array}$	-0.5372
ROYAL A	$\mathscr{I}G(\rho)$	32 °	$\begin{array}{c} -0.6963\\ .6939\\ .6939\\ .6914\\ .6887\\ .6858\end{array}$	$\begin{array}{c} -0.6829\\ \cdot 6798\\ \cdot 6766\\ \cdot 6733\\ \cdot 6699\end{array}$	$\begin{array}{c} -0.6663\\ \cdot 6627\\ \cdot 6520\\ \cdot 6530\\ \cdot 6552\\ \cdot 6512\end{array}$	$\begin{array}{c} -0.6473\\ \cdot 6432\\ \cdot 6432\\ \cdot 6390\\ \cdot 6348\\ \cdot 6305\\ \cdot 6305\end{array}$	$\begin{array}{c} -0.6262\\ \cdot 6218\\ \cdot 6174\\ \cdot 6129\\ \cdot 6083\end{array}$	- 0.6037 .5991 .5944 .5897 .5850	$\begin{array}{c} -0.5803\\ \cdot5755\\ \cdot5707\\ \cdot5659\\ \cdot5611\\ \end{array}$	$\begin{array}{c} -0.5563\\ \cdot5514\\ \cdot5514\\ \cdot5466\\ \cdot5418\\ \cdot5369\end{array}$	-0.5321
THE		31 °	$\begin{array}{c} - 0.6901 \\ 0.6876 \\ 0.6850 \\ 0.6822 \\ 0.6793 \\ 0.6793 \end{array}$	$\begin{array}{c} - 0.6763\\ \cdot 6732\\ \cdot 6732\\ \cdot 6700\\ \cdot 6667\\ \cdot 6632\end{array}$	$\begin{array}{c} - \ 0.6597 \\ \cdot \ 6560 \\ \cdot \ 6523 \\ \cdot \ 6485 \\ \cdot \ 6446 \end{array}$	$\begin{array}{c} - 0.6406\\ \cdot 6366\\ \cdot 6324\\ \cdot 6223\\ \cdot 6240\\ \cdot 6240\end{array}$	$\begin{array}{c} - 0.6197\\ \cdot 6154\\ \cdot 6109\\ \cdot 6005\\ \cdot 6020\end{array}$	$\begin{array}{c} - \ 0.5975 \\ \cdot 5929 \\ \cdot 5833 \\ \cdot 5837 \\ \cdot 5790 \\ \cdot 5790 \end{array}$	- 0.5744 .5697 .5650 .5650 .5555	$\begin{array}{c} -0.5508\\ \cdot5460\\ \cdot5413\\ \cdot5365\\ \cdot5318\end{array}$	-0.5271
PHILOSOPHICAL TRANSACTIONS		30 °	$\begin{array}{c} -0.6839\\ 0.6813\\ 0.6787\\ 0.6787\\ 0.6759\\ 0.6729\end{array}$	- 0.6699 .6668 .6635 .6631 .6601	$\begin{array}{c} - 0.6531 \\ \cdot 6495 \\ \cdot 6458 \\ \cdot 6419 \\ \cdot 6381 \\ \cdot 6381 \end{array}$	$\begin{array}{c} -0.6341\\ \cdot 6301\\ \cdot 6301\\ \cdot 6260\\ \cdot 6218\\ \cdot 6176\end{array}$	$\begin{array}{c} - 0.6133 \\ \cdot 6090 \\ \cdot 6047 \\ \cdot 6003 \\ \cdot 5958 \end{array}$	$\begin{array}{c} - 0.5914 \\ \cdot 5868 \\ \cdot 5823 \\ \cdot 5778 \\ \cdot 5732 \end{array}$	- 0.5686 .5640 .5533 .5533 .5547	$\begin{array}{c} -0.5454\\ \cdot5407\\ \cdot5407\\ \cdot5361\\ \cdot5314\\ \cdot5268\\ \cdot5268\end{array}$	-0.5221
PH TR/		34 °	+0.1996 $\cdot 1903$ $\cdot 1811$ $\cdot 1720$ $\cdot 1631$	+0.1543 $\cdot 1457$ $\cdot 1371$ $\cdot 1205$ $\cdot 1205$	+0.1124 $\cdot 1045$ $\cdot 0967$ $\cdot 0890$ $\cdot 0815$	+0.0741 0.0669 0.0598 0.0529 0.461	+0.0394 0.0329 0.0266 0.0266 0.0204	+0.0085 +0.0027 -0.0029 -0.0084 $\cdot0137$	$\begin{array}{c} - \ 0.0189 \\ \cdot \ 0.240 \\ \cdot \ 0.289 \\ \cdot \ 0.337 \\ \cdot \ 0.383 \end{array}$	$\begin{array}{c} - 0.0428 \\ \cdot 0472 \\ \cdot 0515 \\ \cdot 0556 \\ \cdot 0556 \end{array}$	-0.0634
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		33 °	+ 0.2011 -1920 -1829 -1740 -1740 -1653	+0.1566 $\cdot 1481$ $\cdot 1398$ $\cdot 1315$ $\cdot 1235$	+ 0.1155 $\cdot 1077$ $\cdot 1001$ $\cdot 0926$ $\cdot 0852$	+ 0-0780 -0709 -0640 -0572 -0506	+0-0441 -0377 -0315 -0255 -0196	+0.0138 $\cdot0082$ +0.0027 -0.0027 $\cdot0079$	$\begin{array}{c} - \ 0.0130 \\ \cdot \ 0.179 \\ \cdot \ 0.227 \\ \cdot \ 0.274 \\ \cdot \ 0.319 \end{array}$	- 0-0363 -0406 -0448 -0488 -0527	-0.0565
A	$\mathscr{R}G(ho)$	3 3 °	+0.2028 $\cdot 1937$ $\cdot 1848$ $\cdot 1761$ $\cdot 1675$	+0.1590 $\cdot1506$ $\cdot1424$ $\cdot1344$ $\cdot1264$	+0-1186 -1110 -1035 -0961 -0889	+0.0819 0.749 -0682 -0615 -0550	+0-0487 -0425 -0364 -0305 -0247	+0.0190 -0135 -0082 +0.0029 -0.0021	$\begin{array}{c} - \ 0.0071 \\ - \ 0.0119 \\ - \ 0.0166 \\ - \ 0.0212 \\ - \ 0.256 \end{array}$	$\begin{array}{c} - \ 0.0299 \\ 0.341 \\ 0.382 \\ 0.382 \\ 0.421 \\ 0.460 \end{array}$	-0.0497
E ROYAL CIETY	02	31 °	+0.2044 -1955 -1868 -1868 -1782 -1697	+0-1614 -1532 -1451 -1372 -1372	+0.1218 .1143 .1069 .0997 .0926	+0-0857 -0789 -0723 -0658 -0594	+0-0532 -0472 -0412 -0354 -0354	+0.0242 -0189 -0136 -0085 +0.0035	$\begin{array}{c} -0.0013\\ \cdot 0061\\ \cdot 0107\\ \cdot 0151\\ \cdot 0195\end{array}$	-0.0237 -0.278 -0.218 -0.316 -0.356 -0.394	-0.0430
HICAL THE		ρ 30°	+0.2061 -1974 -1888 -1888 -1803 -1720	+0.1638 .1557 .1478 .1478 .1400	+0.1249 $\cdot 1176$ $\cdot 1103$ $\cdot 1033$ $\cdot 0963$	+0-0896 -0829 -0764 -0700	+0.0577 .0518 .0460 .0403 .0348	+0-0294 -0241 -0190 -0140 -0091	+0.0043 -0.0003 -0048 -0042 -0092	-0.0175 -0.216 -0.254 -0.292 -0.329	-0.0364
PHILOSOPHICAL TRANSACTIONS		$ \rho $	0.40 41 42 43	0.45 46 47 47 48	0.50 51 53 53 54	0. 90 90 90 90 90 90 90 90 90 90 90 90 90	0-60 61 65 65 64 64	0-65 66 63 69 69	0.70 .71 .72 .73 .73	0.75 77 77 78	0.80

Downloaded from rsta.royalsocietypublishing.org

ON THE COMPLEX VALUES OF ρ

207

25-2

	208		P. C. CLEMMOW AND CARA M. MUNFORD								
NEERING		39°	0.6267 	$\begin{array}{c} - 0.6631 \\ 0.6697 \\ 0.6760 \\ 0.6760 \\ 0.6820 \\ 0.6878 \end{array}$	$\begin{array}{c} -0.6934 \\ 0.6986 \\ 0.7037 \\ 0.7084 \\ 0.7130 \\ 0.7130 \end{array}$	$\begin{array}{c} -0.7172\\ .7212\\ .7249\\ .7284\\ .7316\\ .7316\end{array}$	- 0.7346 .7373 .7398 .7420 .7439	$\begin{array}{c} -0.7456\\ .7471\\ .7471\\ .7483\\ .7493\\ .7500\end{array}$	$\begin{array}{r} -0.7505 \\ .7508 \\ .7508 \\ .7508 \\ .7506 \\ .7502 \end{array}$	$\begin{array}{c} -0.7496\\ \cdot 7487\\ \cdot 7487\\ \cdot 7477\\ \cdot 7464\\ \cdot 7450\\ \cdot 7450\end{array}$	-0.7433
		38 °	-0-6267 -6343 -6416 -6487 -6556	-0.6622 -6686 -6747 -6805 -6861	$\begin{array}{c} - 0.6915 \\ \cdot 6965 \\ \cdot 7014 \\ \cdot 7059 \\ \cdot 7102 \\ \cdot 7102 \end{array}$	-0.7143 .7181 .7216 .7249 .7279	- 0.7307 .7332 .7354 .7354 .7374	$\begin{array}{c} -0.7407\\ \cdot 7420\\ \cdot 7430\\ \cdot 7439\\ \cdot 7444\\ \cdot 7444\end{array}$	- 0-7448 .7449 .7448 .7448 .7444	$\begin{array}{c} -0.7431\\ \cdot 7421\\ \cdot 7410\\ \cdot 7396\\ \cdot 7380\end{array}$	-0.7363
CIETY	$\mathscr{I} G(\rho)$	37 °	-0.6267 -0.6261 -6341 -6413 -6482 -6549	- 0-6613 -6674 -6734 -6790 -6844	- 0-6896 -6944 -6990 -7034 -7075	-0.7114 $\cdot 7149$ $\cdot 7183$ $\cdot 7213$ $\cdot 7242$	$\begin{array}{c} -0.7267\\ \cdot 7291\\ \cdot 7311\\ \cdot 7330\\ \cdot 7345\\ \cdot 7345\end{array}$	-0.7359 .7370 .7378 .7385 .7385 .7389	-0.7391 $\cdot7390$ $\cdot7388$ $\cdot7383$ $\cdot7383$ $\cdot7376$	-0.7367 .7356 .7344 .7329 .7312	-0.7294
SOC		36°	-0.6267 -6339 -6409 -6476 -6541	- 0.6603 .6663 .6720 .6775 .6827	-0.6876 .6923 .6967 .7009 .7048	-0.7084 $\cdot 7118$ $\cdot 7149$ $\cdot 7178$ $\cdot 7178$	-0.7228 .7250 .7268 .7285 .7299	$\begin{array}{c} -0.7311 \\ \cdot 7320 \\ \cdot 7327 \\ \cdot 7332 \\ \cdot 7332 \\ \cdot 7334 \end{array}$	$\begin{array}{c} -0.7335\\ \cdot 7333\\ \cdot 7329\\ \cdot 7329\\ \cdot 7323\\ \cdot 7323\\ \cdot 7315\end{array}$	$\begin{array}{c} -0.7304 \\ \cdot 7292 \\ \cdot 7278 \\ \cdot 7263 \\ \cdot 7263 \\ \cdot 7245 \end{array}$	-0.7225
		35°	- 0.6267 -6337 -6405 -6471 -6534	$\begin{array}{c} -0.6594\\ .6652\\ .6707\\ .6760\\ .6810\\ .6810\end{array}$	$\begin{array}{c} -0.6857\\ .6902\\ .6944\\ .6944\\ .6983\\ .7020\end{array}$	-0-7055 -7087 -7116 -7143 -7167	-0.7189 .7209 .7226 .7240 .7253	-0.7263 .7270 .7276 .7276 .7279 .7280	-0.7279 .7276 .7270 .7263 .7263 .7254	-0.7242 .7229 .7214 .7197 .7179	-0.7158
- 1		39°	+0.6267 .6168 .6069 .5968 .5866	+ 0.5762 .5657 .5552 .55445 .5337	+0.5229 .5119 .5009 .4899 .4788	+ 0.4676 .4564 .4451 .4451 .4339 .4226	+ 0-4113 -4000 -3886 -3773 -3773	+ 0.3548 .3436 .3324 .3212 .3212 .3101	+0.2990 -2880 -2771 -2663 -2555	+ 0-2448 -2342 -2236 -2132 -2029	+0.1927
ENGINEERING :IENCES		38 °	+0.6267 -6167 -6066 -5964 -5861	+ 0.5756 .5651 .5544 .544 .5437 .5329	+0.5220 .5110 .4999 .4888 .4888 .4777	+0-4665 -4553 -4441 -4441 -4216 -4216	+0-4103 -3990 -3878 -3765 -3765 -3653	+0.3541 -3430 -3319 -3208 -3208	+0.2989 -2880 -2772 -2665 -2558	+ 0-2453 -2348 -2244 -2141 -2141	+0.1939
	$\mathscr{R} G(ho)$	37°	+0.6267 -6166 -6064 -5961 -5856	+ 0.5751 .5644 .5537 .5320 .5320	+ 0.5211 .5100 .4990 .4879 .4767	+ 0.4655 -4543 -4431 -4431 -4319 -4206	+ 0-4094 -3982 -3870 -3870 -3758 -3647	+0.3536 .3425 .3315 .3205 .3096	+0-2988 -2880 -2774 -2668 -2562	+0.2458 -2355 -2253 -2152 -2051	+0.1952
SOCIETY	0	36°	+0.6267 .6165 .6061 .5957 .5852	+0.5745 .5638 .5530 .5421 .5312	+0.5202 .5091 .4981 .4869 .4758	+0.4646 $\cdot4534$ $\cdot4422$ $\cdot4422$ $\cdot4310$ $\cdot4198$	+ 0.4086 ·3974 ·3863 ·3752 ·3641	+ 0.3531 -3421 -3312 -3312 -3203 -3095	+0-2988 -2882 -2776 -2671 -2568	+0-2465 -2363 -2262 -2162 -2162 -2064	+0.1966
		o 35 °	+0.6267 0.6163 0.059 0.5954 0.5847	+0.5740 .5632 .5523 .5514 .523 .5304	$\begin{array}{c} + 0.5194 \\ \cdot 5083 \\ \cdot 5083 \\ \cdot 4972 \\ \cdot 4860 \\ \cdot 4749 \end{array}$	+ 0.4637 $\cdot 4525$ $\cdot 4413$ $\cdot 4301$ $\cdot 4190$	+ 0.4078 .3967 .3856 .3746 .3636	+0.3527 $\cdot3418$ $\cdot3309$ $\cdot3202$ $\cdot3095$	+0.2989 -2884 -2779 -2676 -2573	+ 0-2472 -2371 -2272 -2272 -2174 -2077	+0.1981
		$ \rho $	0-00 01 02 04	0.05 06 06 09 09	0-10 -11 -12 -13 -14	0-15 -16 -17 -18 -19	0-20 21 23 24	0:25 26 28 28 29	0:30 :31 :33 :33 :34	0:35 36 37 38 37 39	0-40

TRANSACTIONS COCTETV

TRANSACTIONS COCTETV

					ON THE	COMPLEX	K VALUES	S OF p		209	
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		3 9°	- 0.7433 .7415 .7394 .7372 .7372 .7348	-0.7322 .7295 .7266 .7266 .7235 .7203	-0.7169 $\cdot 7134$ $\cdot 7098$ $\cdot 7060$ $\cdot 7020$	0-6980 -6938 -6896 -6852 -6852	-0.6761 .6714 .6666 .6618 .6618 .6568	0-6518 6467 6416 6416 6364 6311	-0.6258 -6204 -6120 -6096 -6041	- 0.5986 .5930 .5875 .5819 .5819	-0.5707
V		38 °	-0.7363 $\cdot7343$ $\cdot7322$ $\cdot7299$ $\cdot7274$	-0.7248 $\cdot 7220$ $\cdot 7190$ $\cdot 7159$ $\cdot 7127$	- 0.7093 .7057 .7020 .6982 .6943	-0.6903 .6861 .6818 .6818 .6775 .6730	$\begin{array}{c} -0.6685\\ .6638\\ .6638\\ .6591\\ .6543\\ .6494\end{array}$	- 0.6444 -6394 -6343 -6343 -6292 -6240	-0.6188 .6135 .6082 .6029 .5975	$\begin{array}{c} -0.5921\\ .5866\\ .5812\\ .5757\\ .5702\\ \end{array}$	-0.5648
THE ROYAL Society	$\mathscr{I} G(\rho)$	37°	$\begin{array}{c} -0.7294 \\ \cdot 7273 \\ \cdot 7251 \\ \cdot 7227 \\ \cdot 7202 \end{array}$	$\begin{array}{c} -0.7175 \\ .71146 \\ .7116 \\ .7085 \\ .7052 \end{array}$	-0.7017 .6982 .6945 .6945 .6907 .6867	- 0.6827 .6786 .6743 .6743 .6655	$\begin{array}{c} - 0.6610 \\ .6564 \\ .6517 \\ .6517 \\ .6470 \\ .6421 \end{array}$	$\begin{array}{c} -0.6372\\ .6323\\ .6323\\ .6273\\ .6222\\ .6171\end{array}$	$\begin{array}{c} -0.6120\\ \cdot 6068\\ \cdot 6016\\ \cdot 5963\\ \cdot 5910\end{array}$	- 0.5857 .5804 .5751 .5697 .5643	-0.5590
		36°	-0.7225 $\cdot 7204$ $\cdot 7181$ $\cdot 7157$ $\cdot 7131$	$\begin{array}{c} - \ 0.7103 \\ \cdot 7074 \\ \cdot 7043 \\ \cdot 7011 \\ \cdot 6978 \end{array}$	$\begin{array}{c} - \ 0.6944 \\ \cdot \ 6908 \\ \cdot \ 6871 \\ \cdot \ 6833 \\ \cdot \ 6793 \end{array}$	$\begin{array}{c} - \ 0.6753 \\ .6712 \\ .6669 \\ .6626 \\ .6582 \\ .6582 \end{array}$	$\begin{array}{c} - \ 0.6537 \\ .6492 \\ .6445 \\ .6398 \\ .6350 \end{array}$	$\begin{array}{c} - 0.6302 \\ \cdot 6253 \\ \cdot 6204 \\ \cdot 6154 \\ \cdot 6104 \end{array}$	$\begin{array}{c} - \ 0.6053 \\ \cdot \ 6002 \\ \cdot \ 5951 \\ \cdot \ 5899 \\ \cdot \ 5848 \end{array}$	$\begin{array}{c} - \ 0.5796 \\ \cdot 5743 \\ \cdot 5691 \\ \cdot 5639 \\ \cdot 5586 \\ \cdot 5586 \end{array}$	-0.5534
PHILOSOPHICAL TRANSACTIONS		32°	-0.7158 .7136 .7113 .7088 .7061	$\begin{array}{c} - 0.7033 \\ \cdot 7003 \\ \cdot 6972 \\ \cdot 6940 \\ \cdot 6906 \end{array}$	$\begin{array}{c} - 0.6871 \\ \cdot 6835 \\ \cdot 6835 \\ \cdot 6798 \\ \cdot 6760 \\ \cdot 6721 \end{array}$	$\begin{array}{c} - 0.6681 \\ \cdot 6639 \\ \cdot 6537 \\ \cdot 6554 \\ \cdot 6511 \end{array}$	$\begin{array}{c} -0.6466\\ .6421\\ .6421\\ .6375\\ .6328\\ .6281\\ .6281\end{array}$	$\begin{array}{c} -0.6234\\ \cdot 6185\\ \cdot 6137\\ \cdot 6038\\ \cdot 6038\end{array}$	- 0.5988 .5938 .5938 .5888 .5786	$- \begin{array}{c} 0.5735 \\ \cdot 5684 \\ \cdot 5633 \\ \cdot 5531 \\ \cdot 5530 \end{array}$	-0.5479
		30°	+0.1927 $\cdot 1825$ $\cdot 1726$ $\cdot 1627$ $\cdot 1529$	+0.1433 $\cdot 1338$ $\cdot 1244$ $\cdot 1152$ $\cdot 1061$	+0.0971 0.0883 0.0796 0.0711 0.0711	+0.0545 -0464 -0385 -0307 -0231	$\begin{array}{r} + \ 0.0156 \\ - \ 0.083 \\ + \ 0.0012 \\ - \ 0.0058 \\ - \ 0.0126 \end{array}$	$\begin{array}{c} - 0.0193 \\ \cdot 0.258 \\ \cdot 0.321 \\ \cdot 0.383 \\ \cdot 0.444 \\ \end{array}$	$\begin{array}{c} - \ 0.0502 \\ - \ 0.560 \\ - \ 0.615 \\ - \ 0.669 \\ - \ 0.722 \end{array}$	$\begin{array}{c} - \ 0.0773 \\ 0.822 \\ 0.870 \\ 0.917 \\ 0.962 \end{array}$	-0.1006
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		38 °	$\begin{array}{c} + 0.1939 \\ \cdot 1840 \\ \cdot 1741 \\ \cdot 1644 \\ \cdot 1549 \end{array}$	+0-1454 -1361 -1269 -1178 -1178	+0-1001 -0915 -0830 -0747 -0747	+0.0584 0505 0428 0352 0352	+0.0205 -0133 +0.0064 -0.0004 -0071	$\begin{array}{c} -0.0136\\ 0.0199\\ 0.0261\\ 0.0322\\ 0.0381\end{array}$	$\begin{array}{c} -0.0438\\ -0.494\\ 0548\\ 0548\\ 0600\\ 0652\end{array}$	- 0.0701 - 0750 - 0796 - 0842 - 0886	-0.0928
V	$\mathscr{R} G(ho)$	37°	+0.1952 $\cdot 1855$ $\cdot 1758$ $\cdot 1663$ $\cdot 1568$	+0.1476 -1384 -1294 -1205 -1118	+0-1032 -0947 -0864 -0782 -0702	+0.0623 -0546 -0471 -0396 -0324	+0.0253 -0183 -0115 +0.0049 -0.0016	- 0.0080 -0142 -0202 -0261 -0318	-0.0374 -0428 -0481 -0533 -0583	- 0.0631 -0678 -0724 -0768 -0811	-0.0852
THE ROYAI Society		36°	+ 0.1966 $\cdot 1870$ $\cdot 1775$ $\cdot 1681$ $\cdot 1589$	+0.1498 $\cdot 1408$ $\cdot 1319$ $\cdot 1232$ $\cdot 1147$	+0.1062 -0980 -0898 -0818 -0818	+0.0663 -0587 -0513 -0411 -0370	+0.0300 -0232 -0166 -0101 +0.0038	-0-0024 -0085 -0144 -0201	$\begin{array}{c} -0.0311\\ 0.365\\ 0.365\\ 0.416\\ 0.466\\ 0.515\end{array}$	-0.0562 -0608 -0653 -0696 -0738	-0.0778
TRANSACTIONS		p 35°	+0.1981 -1886 -1793 -1701 -1610	+0.1520 $\cdot 1432$ $\cdot 1345$ $\cdot 1260$ $\cdot 1176$	+0-1093 -1012 -0932 -0854 -0777	+0-0702 -0628 -0556 -0415	+0-0348 -0281 -0216 -0153 -0091	+0.0030 -0.0029 -0.086 -0142 -0197	- 0.0250 - 0302 - 0401 - 0448	-0-0495 -0539 -0583 -0683 -0666	-0.0705
PHILOS TRANS.		$\left \rho\right ^{\operatorname{arg}}$	040 41 42 43 43 43	0.45 .46 .47 .48	0.50 .51 .53 .53 .53	0:55 56 57 58 59	0.60 61 63 64	0-65 66 63 69	0-70 -71 -72 -73 -74	0.75 .76 .77 .78 .79	0.80

			210	P. C.	CLEMMO	OW AND C	CARA M. I	MUNFORI)		
L, IG		45 °	$\begin{array}{c} -0.6267\\ .6354\\ .6354\\ .6440\\ .6523\\ .6605\end{array}$	$\begin{array}{c} -0.6684 \\ .6761 \\ .6781 \\ .6836 \\ .6908 \\ .6978 \end{array}$	-0.7046 .7111 .7174 .7234 .7292	$\begin{array}{c} - \ 0.7347 \\ \cdot 7400 \\ \cdot 7450 \\ \cdot 7498 \\ \cdot 7543 \end{array}$	$\begin{array}{c} - \ 0.7585 \\ \cdot 7625 \\ \cdot 7662 \\ \cdot 7696 \\ \cdot 7728 \end{array}$	$\begin{array}{c} - \ 0.7757 \\ \cdot 7783 \\ \cdot 7807 \\ \cdot 7807 \\ \cdot 7828 \\ \cdot 7828 \\ \cdot 7846 \end{array}$	$\begin{array}{c} -0.7862 \\ \cdot 7875 \\ \cdot 7876 \\ \cdot 7886 \\ \cdot 7894 \\ \cdot 7900 \end{array}$	-0.7903 .7903 .7903 .7897 .7890	-0.7881
MATHEMATICAL, PHYSICAL & ENGINEERING SCIENCES		44°	$\begin{array}{c} -0.6267\\ .6353\\ .6353\\ .6437\\ .6518\\ .6598\\ .6598\end{array}$	$\begin{array}{c} - 0.6675 \\ .6751 \\ .6751 \\ .6823 \\ .6894 \\ .6962 \end{array}$	$\begin{array}{c} -0.7028\\ .7091\\ .7151\\ .71210\\ .7265\end{array}$	$\begin{array}{c} -0.7318 \\ \cdot 7369 \\ \cdot 7417 \\ \cdot 7462 \\ \cdot 7505 \end{array}$	-0.7545 .7582 .7617 .7619 .7679	-0.7706 .7730 .7752 .7771 .7771	$\begin{array}{c} -0.7801\\ \cdot 7813\\ \cdot 7821\\ \cdot 7821\\ \cdot 7828\\ \cdot 7831\end{array}$	-0.7833 .7831 .7828 .7828 .7828 .7814	-0.7803
V TV	$\mathscr{I} G(\rho)$	43°	$\begin{array}{c} -0.6267\\ \cdot 6351\\ \cdot 6351\\ \cdot 6433\\ \cdot 6513\\ \cdot 6591\\ \cdot 6591\end{array}$	$\begin{array}{c} - \ 0.6667 \\ .6740 \\ .6741 \\ .6811 \\ .6879 \\ .6945 \end{array}$	$\begin{array}{c} -0.7009\\ .7070\\ .7129\\ .7185\\ .7238\\ .7238\end{array}$	-0.7289 .7337 .7383 .7383 .7426 .7467	$\begin{array}{c} -0.7505\\ .7540\\ .7573\\ .7573\\ .7603\\ .7630\end{array}$	-0.7655 .7677 .7697 .7714 .7729	$\begin{array}{c} -0.7741\\ \cdot 7750\\ \cdot 7757\\ \cdot 7762\\ \cdot 7762\\ \cdot 7764\end{array}$	$\begin{array}{c} -0.7763\\ .7761\\ .7756\\ .7756\\ .7739\\ .7739\end{array}$	-0-7727
THE ROYAL SOCIETY	2	43 °	$\begin{array}{c} -0.6267\\ \cdot 6349\\ \cdot 6343\\ \cdot 6430\\ \cdot 6508\\ \cdot 6584\end{array}$	$\begin{array}{c} -0.6658\\ .6729\\ .6729\\ .6798\\ .6865\\ .6929\end{array}$	$\begin{array}{c} -0.6990\\ \cdot 7049\\ \cdot 7106\\ \cdot 7116\\ \cdot 7211\\ \cdot 7211\end{array}$	$\begin{array}{c} - \ 0.7260 \\ .7306 \\ .7350 \\ .7351 \\ .7391 \\ .7429 \end{array}$	- 0.7465 .7498 .7529 .7557 .7582	$\begin{array}{c} - \ 0.7605 \\ .7625 \\ .7643 \\ .7658 \\ .7671 \\ .7671 \end{array}$	-0.7681 .7689 .7694 .7697 .7697	-0.7695 .7691 .7684 .7684 .7676 .7665	-0.7651
HICAL TF		41 °	- 0-6267 -6348 -6328 -6427 -6503 -6577	$\begin{array}{c} - 0.6649\\ \cdot 6718\\ \cdot 6718\\ \cdot 6785\\ \cdot 6850\\ \cdot 6912\end{array}$	-0.6972 $\cdot 7028$ $\cdot 7083$ $\cdot 7135$ $\cdot 7184$	$\begin{array}{c} - \ 0.7231 \\ .7275 \\ .7316 \\ .7355 \\ .7392 \\ .7392 \end{array}$	-0.7425 .7456 .7485 .7485 .7511 .7534	$\begin{array}{c} -0.7555\\ .7573\\ .7573\\ .7589\\ .7603\\ .7613\end{array}$	-0.7622 .7628 .7631 .7631 .7631 .7631	-0.7628 .7622 .7614 .7604 .7592	-0.7578
PHILOSOPHICAL TRANSACTIONS		40 °	$\begin{array}{c} -0.6267\\ .6346\\ .6346\\ .6423\\ .6498\\ .6570\end{array}$	$\begin{array}{c} -0.6640\\ \cdot 6708\\ \cdot 6773\\ \cdot 6835\\ \cdot 6835\\ \cdot 6895\end{array}$	$\begin{array}{c} -0.6953\\ \cdot 7008\\ \cdot 7008\\ \cdot 7110\\ \cdot 7117\\ \cdot 7157\end{array}$	$\begin{array}{c} - \ 0.7201 \\ \cdot 7243 \\ \cdot 7283 \\ \cdot 7283 \\ \cdot 7320 \\ \cdot 7354 \end{array}$	- 0.7386 .7415 .7441 .7441 .7465 .7487	$\begin{array}{c} -0.7505\\ .7522\\ .7536\\ .7536\\ .7556\\ .7556\end{array}$	- 0.7563 .7567 .7569 .7569 .7566	$\begin{array}{c} -0.7561 \\ .7554 \\ .7545 \\ .7545 \\ .7534 \\ .7520 \end{array}$	-0.7505
		45°	+ 0.6267 -6177 -6085 -5992 -5897	+ 0.5800 + 0.5701 - 5701 - 5500 - 55396 - 53396	+0.5292 .5186 .5079 .4970 .4861	+ 0.4750 + 4639 -4527 -4413 -4413 -4300	+ 0.4185 $\cdot 4070$ $\cdot 3954$ $\cdot 3838$ $\cdot 3721$	+0.3605 $\cdot3487$ $\cdot3370$ $\cdot3253$ $\cdot3136$	+ 0.3019 -2902 -2785 -2669 -2552	+ 0.2437 -2322 -2207 -2093 -1980	+0.1867
THEMATICAL, YSICAL ENGINEERING ENCES		44 °	+0.6267 -6176 -6083 -5988 -5891	+0.5793 $\cdot 5694$ $\cdot 5592$ $\cdot 5490$ $\cdot 5386$	+ 0.5281 .5174 .5066 .4957 .4847	+0.4737 $\cdot4625$ $\cdot4512$ $\cdot4399$ $\cdot4399$ $\cdot4285$	+ 0.4171 $\cdot 4056$ $\cdot 3941$ $\cdot 3825$ $\cdot 3709$	+ 0.3593 $\cdot 3477$ $\cdot 3360$ $\cdot 3244$ $\cdot 3128$	+ 0.3012 -2896 -2780 -2665 -2550	+0.2436 $\cdot 2323$ $\cdot 2210$ $\cdot 2097$ $\cdot 1986$	+0.1875
ATH PHYSI & ENG & ENG		43 °	+0.6267 .6174 .6080 .5984 .5886	+ 0.5787 .5686 .5584 .5480 .5375	+0.5269 .5162 .5054 .4945 .4834	+ 0.4723 $\cdot 4611$ $\cdot 4499$ $\cdot 4386$ $\cdot 4272$	+ 0.4158 $\cdot 4043$ $\cdot 3928$ $\cdot 3813$ $\cdot 3698$	+0.3582 $\cdot3467$ $\cdot3351$ $\cdot3351$ $\cdot3236$ $\cdot3120$	+ 0.3006 -2891 -2777 -2663 -2663 -2549	+ 0.2437 -2325 -2213 -2102 -1993	+0.1884
THE ROYAL SOCIETY	$\mathscr{R}G(\rho)$	42 °	+ 0.6267 .6173 .6077 .5980 .5881	+ 0.5780 .5679 .5575 .5471 .5365	+ 0.5259 .5151 .5042 .4932 .4822	+ 0.4711 $\cdot 4599$ $\cdot 4486$ $\cdot 4373$ $\cdot 4259$	+ 0.4145 + 0.4031 -3917 -3802 -3687	+0.3572 3458 3343 3328 3228 3114	+0.3000 -2887 -2774 -2661 -2549	$+ \begin{array}{c} 0.2438 \\ \cdot 2327 \\ \cdot 23218 \\ \cdot 2218 \\ \cdot 2109 \\ \cdot 2000 \end{array}$	+0.1893
		41 °	+ 0.6267 -6171 -6074 -5976 -5876	+ 0.5774 .5671 .5567 .5462 .5356	+0.5248 .5140 .5031 .4921 .4810	+ 0.4698 .4586 .4474 .4361 .4247	+0.4134 $\cdot4020$ $\cdot3906$ $\cdot3792$ $\cdot3677$	+ 0.3563 + 0.3563 - 0.3449 - 0.3336 - 0.3336 - 0.3222 - 0.3222 - 0.3109 - 0.3109	+ 0.2996 -2884 -2772 -2661 -2550	+ 0.2440 -2331 -2233 -2223 -2116 -2009	+0.1904
PHILOSOPHICAL TRANSACTIONS		p 40°	+ 0.6267 + 0.6170 - 0.6170 - 0.6071 - 0.6071 - 0.5972 - 0.5871 - 0.5872 - 0.5871 - 0.5872 - 0.5871 - 0.5872 -	+ 0.5768 .5664 .5559 .5453 .5346	$\begin{array}{c} + 0.5238 \\ \cdot 5130 \\ \cdot 5020 \\ \cdot 4910 \\ \cdot 4799 \end{array}$	$\begin{array}{c} + \ 0.4687 \\ \cdot 4575 \\ \cdot 4462 \\ \cdot 4462 \\ \cdot 4349 \\ \cdot 4236 \end{array}$	+0.4123 $\cdot4009$ $\cdot3896$ $\cdot3782$ $\cdot3669$	+0.3555 $\cdot3442$ $\cdot3329$ $\cdot3217$ $\cdot3217$ $\cdot3104$	+ 0.2993 $\cdot 2882$ $\cdot 2771$ $\cdot 2661$ $\cdot 2552$	$+ \begin{array}{c} 0 \cdot 2444 \\ \cdot 2336 \\ \cdot 2229 \\ \cdot 2123 \\ \cdot 2019 \end{array}$	+0.1915
PHILC		$\frac{\arg \rho}{ \rho }$	0.00 0.00 0.00 0.00 0.00	0.05 06 07 09 09	0:10 11 12 13 14	0.15 .16 .17 .18 .19	0:20 21 23 23 24	0:25 :27 :28 :29	0:30 :31 :32 :33 :34	0:35 :36 :37 :38 :39	-0 -40

					ON THE	COMPLEX	K VALUES	OF p		211	
DN		45 °	$\begin{array}{c} -0.7881 \\ .7869 \\ .7855 \\ .7839 \\ .7839 \\ .7821 \end{array}$	$\begin{array}{c} -0.7800\\ .7777\\ .77752\\ .7752\\ .7726\\ .7697\end{array}$	$\begin{array}{c} -0.7666\\ \cdot 7633\\ \cdot 7599\\ \cdot 7562\\ \cdot 7524\\ \end{array}$	$\begin{array}{c} -0.7484 \\ \cdot 7443 \\ \cdot 7400 \\ \cdot 7355 \\ \cdot 7309 \end{array}$	-0.7261 .7212 .7162 .7111 .7058	$\begin{array}{c} -0.7004 \\ \cdot 6949 \\ \cdot 6893 \\ \cdot 6836 \\ \cdot 6778 \end{array}$	$\begin{array}{c} - 0.6720 \\ \cdot 6660 \\ \cdot 6600 \\ \cdot 6539 \\ \cdot 6477 \end{array}$	$\begin{array}{c} - \ 0.6415 \\ \cdot \ 6352 \\ \cdot \ 6352 \\ \cdot \ 6225 \\ \cdot \ 6161 \end{array}$	-0.6097
PHYSICAL & ENGINEERING SCIENCES		44°	- 0.7803 .7775 .7775 .7738 .7738	-0.7717 .7693 .7667 .7667 .7640 .7610		$\begin{array}{c} -0.7395\\ \cdot 7353\\ \cdot 7353\\ \cdot 7310\\ \cdot 7266\\ \cdot 7220\end{array}$	-0.7172 .7124 .7074 .7023 .6971	$\begin{array}{c} - 0.6917 \\ \cdot 6863 \\ \cdot 6808 \\ \cdot 6808 \\ \cdot 6752 \\ \cdot 6695 \end{array}$	$\begin{array}{c} - 0.6637 \\ \cdot 6578 \\ \cdot 6519 \\ \cdot 6519 \\ \cdot 6459 \\ \cdot 6399 \end{array}$	$\begin{array}{c} - 0.6338 \\ \cdot 6277 \\ \cdot 6215 \\ \cdot 6152 \\ \cdot 6090 \end{array}$	-0.6027
A ALA	$\mathscr{I} G(\rho)$	43 °	$\begin{array}{c} -0.7727\\ \cdot 7712\\ \cdot 7696\\ \cdot 7696\\ \cdot 7678\\ \cdot 7657\end{array}$	$\begin{array}{c} -0.7635\\ .7610\\ .7584\\ .7555\\ .7525\\ \end{array}$	$\begin{array}{c} -0.7493\\ .7459\\ .7459\\ .7424\\ .7387\\ .7348\end{array}$	$\begin{array}{c} -0.7308\\ \cdot 7266\\ \cdot 7223\\ \cdot 7179\\ \cdot 7133\\ \cdot 7133\end{array}$	- 0.7086 .7037 .6988 .6937 .6886	$\begin{array}{c} - \ 0.6833 \\ .6780 \\ .6780 \\ .6725 \\ .6670 \\ .6614 \end{array}$	$\begin{array}{c} - 0.6557 \\ .6499 \\ .6441 \\ .6383 \\ .6323 \\ .6323 \end{array}$	$\begin{array}{c} - \ 0.6264 \\ .6203 \\ .6143 \\ .6082 \\ .6021 \\ .6021 \end{array}$	-0.5959
OCIET	2	42 °	$\begin{array}{c} -0.7651\\ .7636\\ .7619\\ .7599\\ .7578\end{array}$	$\begin{array}{c} -0.7554 \\ .7529 \\ .7502 \\ .7473 \\ .7442 \\ .7442 \end{array}$	$\begin{array}{c} -0.7410\\ .7375\\ .7340\\ .7340\\ .7302\\ .7263\end{array}$	-0.7223 .7181 .7138 .7094 .7048	$\begin{array}{c} -0.7002\\ \cdot 6954\\ \cdot 6904\\ \cdot 6854\\ \cdot 6803\end{array}$	$\begin{array}{c} - \ 0.6751 \\ .6698 \\ .6645 \\ .6590 \\ .6535 \end{array}$	$\begin{array}{c} - \ 0.6479 \\ .6422 \\ .6365 \\ .6308 \\ .6308 \\ .6250 \end{array}$	$\begin{array}{c} - 0.6191 \\ \cdot 6132 \\ \cdot 6073 \\ \cdot 6013 \\ \cdot 5953 \end{array}$	-0.5893
TIONS S		41 °	-0.7578 .7561 .7543 .7522 .7500	$-\frac{0.7476}{.7450}$ -7450 -7422 -7392 -7361	$\begin{array}{c} -0.7328\\ \cdot 7293\\ \cdot 7257\\ \cdot 7257\\ \cdot 7220\\ \cdot 7181\\ \cdot 7181\end{array}$	$\begin{array}{c} -0.7140\\ \cdot 7098\\ \cdot 7055\\ \cdot 7011\\ \cdot 6966\end{array}$	$\begin{array}{c} - \ 0.6919 \\ \cdot \ 6872 \\ \cdot \ 6823 \\ \cdot \ 6773 \\ \cdot \ 6723 \\ \cdot \ 6723 \end{array}$	$\begin{array}{c} - \ 0.6672 \\ .6619 \\ .6566 \\ .6513 \\ .6513 \\ .6458 \end{array}$	$\begin{array}{c} - 0.6403 \\ .6348 \\ .6348 \\ .6292 \\ .6235 \\ .6178 \end{array}$	$\begin{array}{c} - 0.6121 \\ .6063 \\ .6005 \\ .5947 \\ .5888 \end{array}$	-0.5829
TRANSACTIONS		40°	-0.7505 .7487 .7468 .7468 .7447 .7423	-0.7398 .7372 .7343 .7343 .7313 .7281	$\begin{array}{c} -0.7248\\ \cdot 7213\\ \cdot 7176\\ \cdot 7139\\ \cdot 7139\\ \cdot 7100\end{array}$	$\begin{array}{c} -0.7059\\ \cdot 7017\\ \cdot 6975\\ \cdot 6931\\ \cdot 6885\end{array}$	- 0-6839 -6792 -6744 -6695 -6645	- 0.6594 .6542 .6490 .6437 .6384	$\begin{array}{c} - \ 0.6330 \\ .6275 \\ .6220 \\ .6164 \\ .6109 \end{array}$	$\begin{array}{c} - 0.6052 \\ .5996 \\ .5939 \\ .5882 \\ .5825 \\ .5825 \end{array}$	-0.5767
		45°	+0.1867 -1756 -1645 -1635 -1535 -1426	+0.1318 $\cdot 1212$ $\cdot 1106$ $\cdot 1002$ $\cdot 0899$	+ 0.0797 - 0696 - 0597 - 0500 - 0404	$\begin{array}{c} + 0.0309 \\ - 0.216 \\ - 0.124 \\ + 0.0034 \\ - 0.0055 \end{array}$	$\begin{array}{c} -0.0141\\ -0.226\\ 0.0310\\ 0.392\\ 0.472\end{array}$	- 0.0550 -0626 -0701 -0774 -0845	$\begin{array}{c} -0.0915\\ \cdot0.0982\\ \cdot1048\\ \cdot1112\\ \cdot1174\end{array}$	$\begin{array}{c} - \ 0.1235 \\ \cdot 1293 \\ \cdot 1293 \\ \cdot 1350 \\ \cdot 1405 \\ \cdot 1459 \end{array}$	-0.1510
SICAL NGINEERING ENCES		44°	+0.1875 $\cdot 1765$ $\cdot 1656$ $\cdot 1548$ $\cdot 1548$ $\cdot 1442$	+0.1336 $\cdot 1231$ $\cdot 1128$ $\cdot 1025$ $\cdot 0925$	+0.0825 0.727 0.630 0.534 0.534	+ 0.0348 + 0.0348 - 0.257 - 0.168 + 0.0080 - 0.0060	$\begin{array}{c} - 0.0091 \\ \cdot 0174 \\ \cdot 0255 \\ \cdot 0335 \\ \cdot 0335 \\ \cdot 0412 \end{array}$	$\begin{array}{c} - 0.0489\\ \cdot 0563\\ \cdot 0563\\ \cdot 0636\\ \cdot 0707\\ \cdot 0776\end{array}$	$\begin{array}{c} -0.0843\\ \cdot 0909\\ \cdot 0973\\ \cdot 1035\\ \cdot 1095\end{array}$	$\begin{array}{c} -0.1154\\ \cdot 1211\\ \cdot 12166\\ \cdot 1266\\ \cdot 1319\\ \cdot 1371\end{array}$	-0.1421
		43°	+0.1884 $\cdot 1776$ $\cdot 1669$ $\cdot 1563$ $\cdot 1458$	+0.1354 -1251 $\cdot1150$ $\cdot1050$ $\cdot0951$	+ 0.0853 -0.757 -0.662 -0.569 -0.569	+0.0387 0.298 0.211 0.126 +0.0042	$\begin{array}{c} - \ 0.0041 \\ - \ 0.122 \\ 0.201 \\ 0.278 \\ 0.354 \end{array}$	$\begin{array}{c} - 0.0428 \\ \cdot 0500 \\ \cdot 0571 \\ \cdot 0571 \\ \cdot 0640 \\ \cdot 0707 \end{array}$	-0.0773 -0.836 -0898 -0959 -1017	$\begin{array}{c} -0.1074 \\ \cdot 1130 \\ \cdot 1183 \\ \cdot 1235 \\ \cdot 1235 \\ \cdot 1285 \end{array}$	-0.1334
IETY .	$\mathscr{R}G(\rho)$	42 °	+0.1893 .1787 .1682 .1682 .1578 .1475	+ 0.1373 - 1272 - 1173 - 1074 - 0978	+ 0.0882 -0788 -0696 -0604 -0515	+ 0.0426 -0340 -0255 -0171 -0089	+0.0009 -0.0070 -0147 -0222 -0296	$\begin{array}{c} -0.0368\\ \cdot0439\\ \cdot0507\\ \cdot0574\\ \cdot0574\\ \cdot0640\end{array}$	$\begin{array}{c} -0.0703 \\ \cdot 0765 \\ \cdot 0826 \\ \cdot 0884 \\ \cdot 0941 \end{array}$	$\begin{array}{c} -0.0997\\ \cdot 1050\\ \cdot 1103\\ \cdot 1153\\ \cdot 1153\\ \cdot 1202\end{array}$	-0.1249
		41°	+0.1904 $\cdot 1799$ $\cdot 1696$ $\cdot 1593$ $\cdot 1593$ $\cdot 1492$	+ 0.1392 -1293 -1196 -1100 -1100	+0.0912 -0819 -0729 -0640 -0552	+0.0466 0.381 0.298 0.217 0.217 0.137	+0.0058 -0.0018 -0003 -0167 -0239	$\begin{array}{c} - 0.0309 \\ \cdot 0377 \\ \cdot 0377 \\ \cdot 0444 \\ \cdot 0510 \\ \cdot 0573 \end{array}$	$\begin{array}{c} - \ 0.0635 \\ 0.0696 \\ 0.0754 \\ 0.0811 \\ 0.0867 \end{array}$	$\begin{array}{c} -0.0921\\ \cdot 0973\\ \cdot 1023\\ \cdot 1073\\ \cdot 1120\\ \cdot 1120\end{array}$	-0.1166
TRANSACTIONS		ğρ 40°	+0.1915 -1812 -1710 -1710 -1610 -1610 -1510	+0.1412 $\cdot 1315$ $\cdot 1220$ $\cdot 1125$ $\cdot 1033$	+ 0.0941 - 0.851 - 0.762 - 0.675 - 0.590	+0.0505 -0423 -0342 -0342 -0262 -0184	+0.0108 +0.0033 -0.0040 -0112 0112	$\begin{array}{c} -0.0250\\ \cdot 0317\\ \cdot 0382\\ \cdot 0446\\ \cdot 0508\end{array}$	$\begin{array}{c} -0.0568\\ \cdot0627\\ \cdot0624\\ \cdot0684\\ \cdot0740\\ \cdot0794\end{array}$	$\begin{array}{c} - \ 0.0846 \\ \cdot \ 0897 \\ \cdot \ 0946 \\ \cdot \ 0994 \\ \cdot \ 0994 \\ \cdot \ 1040 \end{array}$	-0.1085
TRA		$\left \rho\right $	040 41 42 43 44	0:45 :46 :47 :48 :48	0:50 51 52 53 54	0.55 56 57 58 59	0.60 61 63 64	0.65 .66 .68 .69	0.70 .71 .72 .73 .74	0.75 .76 .77 .78 .79	0.80

PHILOSOPHICAL THE ROYAL A MATHEMATICAL

PHILOSOPHICAL THE ROYAL A MATHEMATICAL